



HIGH PRECISION BALL BEARINGS

Extra-thin-section Bearings
Flanged Bearings
Stainless-steel Bearings
Bore Dia , 0.6mm to 95mm



Introduction of revised new catalogue EZO-CAT. No. E2301

In recent years, the next-generation technologies such as ICT and robotics are developing at a remarkable speed.

The bearings used in these advanced fields are expected to contribute to light-weight, high-speed, low-vibration, long-life and energy-saving for the machines and the devices, and to have the capability to be applied to a wide variety of applications.

Therefore, we have made a major change to the general catalogue enhancing the convenience for customers which includes but not limited to the following:
 - Added the information of the characteristics of the bearing materials and the necessary information for calculating the bearing life with some calculation examples
 - Enriched the contents of the sections for Fitting, Internal clearance and Lubrication
 - Changed the layout of the product tables for easier searching for the necessary products.

We hope that our revised new catalogue will help you make the best choice of bearings for your various needs.

We will continue to contribute to realizing a sustainable society through providing "EZO Bearings".



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Sapporo Precision group has a policy of complying with Foreign Exchange and Foreign Trade Act and other export-related laws and regulations, and we do not export restricted products and technology in violation of such laws and regulations. Customers are requested to obtain export permissions from authorities when exporting our products which are subject to restrictions.

NOTE1. All information, data and dimension tables in this catalogue have been compiled carefully and have been thoroughly checked. However, no responsibility for damages/losses caused by possible errors or omissions can be assumed.

NOTE2. We reserve the right to change specifications and other information included in this catalogue without notice.

NOTE3. Copyrights to all information on this catalogue belong to our company. Copying of the information is not allowed without prior permission from us.

01 > Bearing Numbering System and Auxiliary Symbols

Material	Radial Clearance	Tolerance Class
<ul style="list-style-type: none"> High Carbon Chromium Bearing Steel SUJ2: No Symbol 	<ul style="list-style-type: none"> Standard deep groove ball bearing: C2, C0 (CN), C3, C4, C5 Miniature / small ball bearings: MC1 0~5µm, MC2 3~8µm, MC3 5~10µm, MC4 8~13µm, MC5 13~20µm, MC6 20~28µm 	<ul style="list-style-type: none"> JIS Class 0: P0 (The symbol may not be displayed) JIS Class 6: P6 JIS Class 5: P5 JIS Class 4: P4 ANSI/ABMA ABEC1: A1 (The symbol may not be displayed) ANSI/ABMA ABEC3: A3 ANSI/ABMA ABEC5: A5 ANSI/ABMA ABEC7: A7 ANSI/ABMA High-precision instrument ball bearing Class 5P: A5P Class 7P: A7P
<ul style="list-style-type: none"> Stainless Steel KS440 (QD51, ACD34): (Outer / Inner rings) SUS440C, ACD34 (Balls) 		
<ul style="list-style-type: none"> Standard Metric Series: H MR, MF, ET and Inch Series: S 		

Bearing Types										
Ex.1			688	H	J	ZZ		MC3		SRL
Ex.2	F		608		TW	2RS		MC4	P6	SRL
Ex.3		MR	52		W	ZZ		MC2	P5	AF2
Ex.4	S	MF	128		W	TTS		MC3	P6	SRL
Ex.5	S	ER	1458		W	ZZS		C0	A3	SRL
Ex.6			6205	H	RJ	2RS		C3		AV2
Ex.7	F		6706		W	2RU		C0		SRL
Ex.8	S	R	144		J	ZZS		MC4	A5P	AF2
Ex.9		R	10		RJ	ZZ	CB	C2		AF2
Ex.10		F	3-8M		TP					AF2

Lubricants	
Main grease brands	
Multiplex SRL (Our standard grease):	SRL
Alvania Grease S2:	AV2
Barrierta L55/2 H1:	L55
Molykote 33M:	M3M
Krytox 240AC:	K24
ISOFLEX SUPER LDS18:	SL8
Beacon 325J:	B32
Main oil brands	
AeroShell Fluid 12 (Our standard oil):	AF2
Windsor Lube L-245X:	WL2
Ceramic Balls [Si ₃ N ₄]:	CB

Seals & Shields	
Teflon Seals with Snap Rings on Both Sides [PTFE]:	TTS
Steel Shields with Snap Rings on Both Sides [SUS304]:	ZZS
Pressed-steel Shields on Both Sides [SPCC, SECC-NC, SUS304]:	ZZ
Contact Rubber Seals on Both Sides [NBR+SPCC]:	2RS
Non-Contact Rubber Seals on Both Sides [NBR+SPCC]:	2RU

Bearing Basic Part No.	
SINGLE ROW DEEP GROOVE BALL BEARING METRIC SERIES:	67, 68, 69, 60, 16, 62, 63
METRIC SERIES BORE DIAMETER NUMBER:	NUMBERS 1-9, DENOTE BORE DIAMETERS IN mm 1X=1.5mm, 2X=2.5mm 00=10mm, 01=12mm, 02=15mm, 03=17mm 04~96: x5 values denote bore dimensions in mm

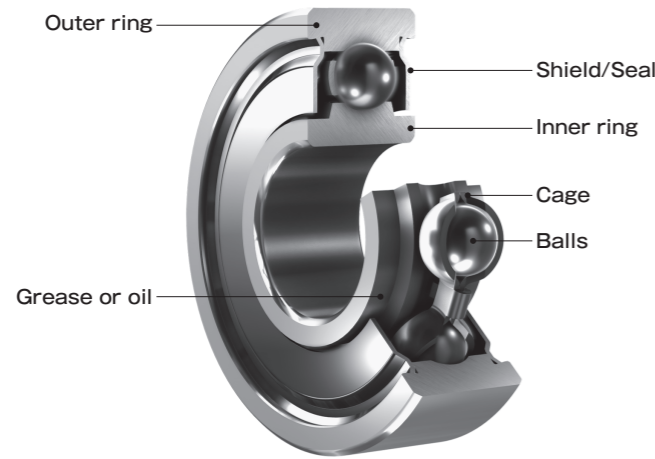
Cages (The symbol may not be displayed)	
Two-Piece Steel Ribbon Type [SPCC, SUS304]:	J
One-Piece Steel Snap Type [SUS304, SUS420J2]:	W
One-Piece Nylon Snap Type [66 nylon]:	TW
Two-Piece Steel Rivet Type [SPCC, SUS304]:	RJ
Full Complement Type (without Cage):	V
Thrust FM Type [SUS304]:	TP
Thrust F Type [brass]:	TD

Following special bearings are also available on certain conditions upon request. Please contact us for details.

- FULL-COMPLEMENT BALL BEARING
- DOUBLE-ROW DEEP GROOVE BEARING
- ANGULAR CONTACT BEARING
- DOUBLE-ROW ANGULAR CONTACT BEARING
- FOUR-POINT CONTACT BEARING
- DUPLEX DEEP GROOVE BEARING
- DUPLEX ANGULAR CONTACT BEARING
- OUTER SURFACE SPECIAL SHAPE BEARING (SPHERICAL SURFACE, R SURFACE, V GROOVE, U GROOVE, etc.)
- HYBRID BEARING (WITH CERAMIC BALLS)

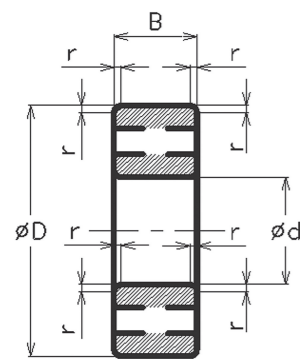
02 > Design and Characteristics of Bearings

Bearing Structure

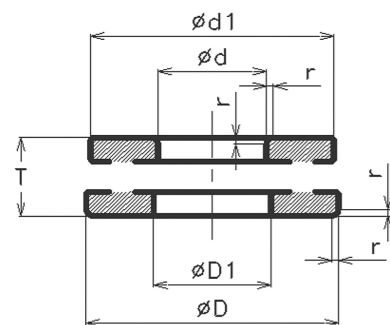


Boundary Dimensions

The boundary dimensions of bearings are the dimensions which indicate the external geometry of a bearing, including the bore diameter d , outside diameter D , width B or height T , and chamfer dimension r . These dimensions are required when mounting a bearing on a shaft or in housings.



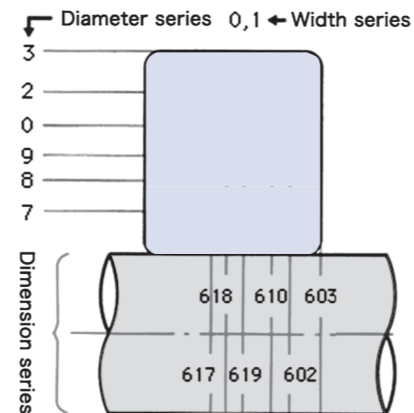
- d : Nominal bore diameter
- D : Nominal outside diameter
- B : Nominal bearing width
- r : Chamfer dimensions of inner ring and outer ring (Minimum value)



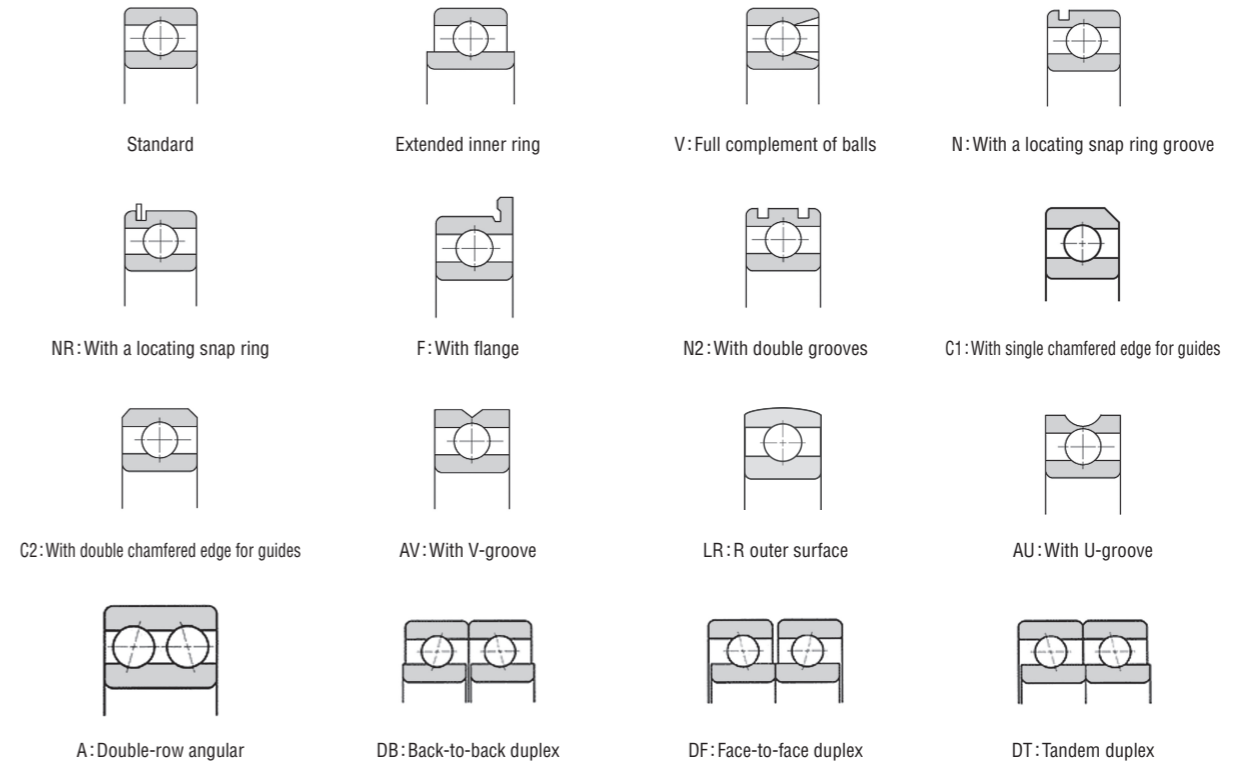
- d : Nominal bore diameter of shaft washer (inner ring)
- $d1$: Nominal outside diameter of shaft washer (inner ring)
- D : Nominal outside diameter of housing washer (outer ring)
- $D1$: Nominal bore diameter of housing washer (outer ring)
- T : Nominal height of bearing
- r : Chamfer dimensions of shaft washer (inner ring) and housing washer (outer ring) (Minimum value)

Difference by Dimension Series of Bearing Cross-Section

The outside diameter and width dimension of the diameter series increase in order from 7 → 3 to the same bore diameter dimension.



Bearing Types



Features of Bearings

Load	Single-row deep groove ball bearings can support an axial load on both sides and moment loads in addition to a radial load. However, full complement ball bearings are for low speed radial loads, and can only support a slight axial load.
Rotational speed	The limiting speed differs by the bearing dimensions, manufacturing accuracy, type of cages, lubrication method, sealing method and load.
Torque and Noise	Single-row deep groove ball bearings manufactured with high accuracy demonstrate low torque and noise.
Inclination of outer ring / inner ring	Inclination occurs between the outer and inner rings of a bearing when there is poor accuracy of the shaft and housing, mounting errors and deflection of the shaft. However, the internal clearance of the bearing will allow such inclination to some extent.
Rigidity	When loads are imposed on a bearing, some elastic deformation occurs in the contact areas between the rolling elements and the raceways. The amount of elastic deformation changes according to the dimensions and type of bearing and the load applied to it, and bearings with larger dimensions demonstrate higher rigidity.
Mounting and Dismounting	Single-row deep groove ball bearings are a non-separable bearing therefore, it is necessary to design the shaft and housing in consideration of periodic inspections and replacement.
Positioning of axial direction	Bearings with flange and locating snap ring are more effective for positioning the axial direction.

Classification by Bearing Dimensions

※Unit:mm

Bearing Classification of Our Company	Nominal bore diameter	Nominal outer diameter
Extra-miniature bearing	$d \leq 2$	$D \leq 7$
Miniature bearing	$d \leq 5$	$D < 9$
Small bearing	$d < 10$	$D \geq 9$
Large bearing	$d \geq 10$	$D \geq 15$

03 > Bearing Materials

For the material of the outer ring, inner ring and balls, high-carbon chromium bearing steel treated with vacuum degassing is used in order to improve the torque and noise level, as well as to extend the bearing life. Also, martensitic stainless steel is used to meet corrosion-resistant requirements.

Chemical Composition of Bearing Materials

Material		High Carbon Chromium Bearing Steel	Stainless Steel			Ceramic
Components		Inner ring, outer ring, balls	Inner ring, outer ring	Balls		Balls
Symbol		SUJ2	KS440 (QD51, ACD34)	SUS440C	ACD34 (Note 1)	Si ₃ N ₄
Chemical composition (Weight %)	C	0.95~1.10	0.60~0.75	0.95~1.20	0.60~0.75	—
	Si	0.15~0.35	≤1.00	≤1.00	≤1.00	—
	Mn	≤0.50	≤1.00	≤1.00	≤1.00	—
	P	≤0.025	≤0.030	≤0.040	≤0.030	—
	S	≤0.025	≤0.020	≤0.030	≤0.020	—
	Cr	1.30~1.60	11.5~13.5	16.0~18.0	11.5~13.5	—
	Mo	≤0.08	≤0.30	≤0.75	≤0.30	—
	Ni	≤0.25	≤0.60	—	≤0.60	—
	Cu	≤0.25	≤0.20	—	≤0.20	—
	V	—	≤0.15	—	≤0.15	—
	Y	—	—	—	—	3.0~4.0
	Al	—	—	—	—	3.2~4.2
Ti	—	—	—	—	0.5~1.0	
Hardness HRC		60~64 (Inner ring, outer ring) 62~67 (Balls)	58~62	59~66		HV1300~2000
Similar steel grades (outside Japan)		SAE52100, 100Cr6, ASTM52100, BS535A99, 1.3505	X65Cr13, 1.4037	SAE51440C, AISI440C, X102CrMo17, X105CrMo17, 1.4125, 1.3543	X65Cr13, 1.4037	—

Note 1: Used for ball diameters of 0.500mm and 0.635mm.

Materials and Characteristics

Material	Raceways and balls	High carbon chromium bearing steel		Stainless steel
	Cages	Low carbon steel plate (SPCC), stainless steel plate (SUS304, SUS420J2)		Polyamide (66 nylon), etc. Stainless steel plate (SUS304, SUS420J2), polyamide (66 nylon), etc.
	Shields	Low carbon steel plate (SPCC, SECC-NC), stainless steel plate (SUS304)		Stainless steel plate (SUS304)
	Seals	Rubber (Nitrile rubber (NBR), fluoro rubber (FKM)) + core plate (SPCC-NP, SECC-NC), PTFE		
Characteristics	Operating temperature	120°C or less (*Up to a maximum of 300°C is possible depending on the dimensional stabilization treatment and/or other specifications)		
	Dynamic load rating	High		About 85% of bearing steel
	Static load rating	High		About 80% of bearing steel
	Friction torque	Low		Slightly higher than bearing steel
	Application	For general use & high precision		For high-speed For corrosion resistance

Physical and Mechanical Properties of Materials

Materials	Specific Gravity	Coefficient of Linear Expansion (1/°C), [0~100°C]	Hardness (Brinell: HB)	Young's Modulus (MPa) (kgf/mm ²)	Tensile Strength (MPa) (kgf/mm ²)	Yield Point (MPa) (kgf/mm ²)	Elongation (%)
SUJ2	7.83	12.5×10 ⁻⁶	650~740	208000 [21200]	1570~1960 [160~200]	—	—
KS440	7.70	10.3×10 ⁻⁶	580	210000 [21400]	1900 [194]	—	—
SUS440C	7.68	10.1×10 ⁻⁶	580	200000 [20400]	1960 [200]	1860 [190]	—
SUS420J2	7.75	10.4×10 ⁻⁶	400	200000 [20400]	1650 [168]	1440 [147]	12
SUS304	7.93	17.3×10 ⁻⁶	150	193000 [19700]	510~657 [52~67]	510~656 [21~32]	50~60
Mild steel (C=0.12~0.2%)	7.86	11.6×10 ⁻⁶	100~130	208000 [21200]	373~471 [38~48]	216~294 [22~30]	24~36
Hard steel (C=0.3~0.5%)	7.84	11.3×10 ⁻⁶	160~200	205000 [20900]	539~686 [55~70]	333~451 [34~46]	14~26
Cast iron	Gray iron FC20	7.30	10.4×10 ⁻⁶	98100 [10000]	167~265 [17~27]	—	—
	Spheroidal graphite cast iron FCD40	7.00	11.7×10 ⁻⁶		120~190		
Copper	8.93	16.2×10 ⁻⁶	50	123000 [12500]	196 [20]	69 [7]	15~20
Brass	(Annealed)	8.50	19.1×10 ⁻⁶	103000 [10500]	294~343 [30~35]	—	65~75
	(Machined)				85~130		363~539 [37~55]
Zinc	7.14	31.0×10 ⁻⁶	30~60	92000 [9400]	147 [15]	—	30~40
Aluminum	2.69	23.7×10 ⁻⁶	15~26	70600 [7200]	78 [8]	34 [3.5]	35
Ceramic (Si ₃ N ₄)	3.20	(2.5~3.3)×10 ⁻⁶	HV1300~2000	245000~314000 [25000~32000]	—	—	—

Comparison Table of SI, CGS and Engineering Units

	Length	Mass	Time	Temperature	Acceleration	Force	Stress	Pressure	Energy	Power
SI	m	kg	s	K	m/s ²	N	Pa	Pa	J	W
CGS System	cm	g	s	°C	Gal	dyn	dyn/cm ²	dyn/cm ²	erg	erg/s
Engineering Unit System	m	kgf·s ² /m	s	°C	m/s ²	kgf	kgf/m ²	kgf/m ²	kgf·m	kgf·m/s

Prefixes of SI Units

Multiples	10 ¹⁸	10 ¹⁵	10 ¹²	10 ⁹	10 ⁶	10 ³	10 ²	10 ¹	10 ⁻¹	10 ⁻²	10 ⁻³	10 ⁻⁶	10 ⁻⁹	10 ⁻¹²	10 ⁻¹⁵	10 ⁻¹⁸
Prefix	Exa	Peta	Tera	Giga	Mega	Kilo	Hecto	Deca	Deci	Centi	Milli	Micro	Nano	Pico	Femto	Ato
Symbols	E	P	T	G	M	k	h	da	d	c	m	μ	n	p	f	a

04 > Types and Characteristics of Cages, Shields and Seals

Cages

W: One-piece Steel Snap Type



The snap type is made by integrally molding stainless steel in press processing. And the inner ring guided design realizes extremely high performance with low torque during low speed rotation.
Standard ball diameter: $\phi 0.5 - \phi 1.588$

J: Two-piece Steel Ribbon Type



For the ribbon type, a ball shaped pocket consists of two parts including a lid side and a claw side, to match the shape of the balls. Generally, this type is ball guided and designed for reducing friction torque during rotation.
Standard ball diameter: $\phi 1.2 - \phi 4.762$

RJ: Two-piece Steel Rivet Type



This type is suitable for larger bearings with high loads applied. Two ribbon shaped parts are riveted together to provide strength against vibration and acceleration. This type is ball guided and designed for reducing the friction torque during rotation.
Standard ball diameter: $\phi 4.762$ or larger

TW: One-piece Nylon Snap Type



The molded nylon cage is ball guided and can endure high-speeds with less fluctuation in the running torque. In addition to the standard type made from 66 nylon, a stronger material containing glass fiber is also available. Operating temperature range (-30 to +120°C).
Standard ball diameter: $\phi 1.2 - \phi 9.525$

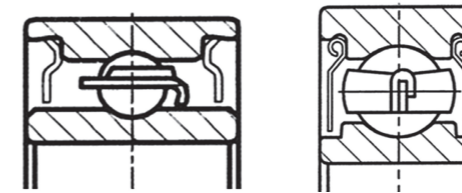
V: Full complement of balls



This type, for low-speed applications, incorporates the maximum number of balls allowed in design to endure a heavy radial load without use of a cage. It can only bear a small axial load because a slot groove is located on the outer ring and the inner ring, respectively.

Shields and Seals

ZZ: Pressed-steel shields

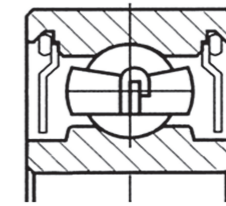


Root shield

Curl shield

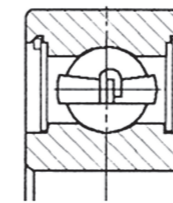
Consists of a structure that presses the steel shields into the outer ring. There is little grease leakage and less intrusion of external contaminants.

ZZS: Steel shields with snap rings



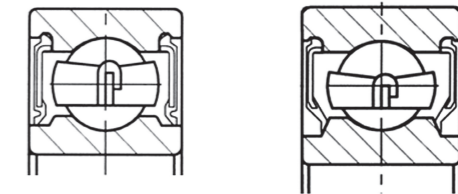
Consists of a structure where steel shields are retained in the outer ring with snap rings. There is less intrusion of external contaminants. This is mainly used for small bearings or thin-section bearings. There is less increase in torque, noises and temperature.

TTS: Teflon seals with snap rings



Consists of a structure where teflon seals reinforced with glass fiber are retained in the outer ring with snap rings. There is less intrusion of external contaminants. This is mainly used for small bearings or thin-section bearings. This structure allows the seal to breathe along with the change in the internal pressure.
Limited operating temperature range: -100 to +260°C

2RS: Contact rubber seals

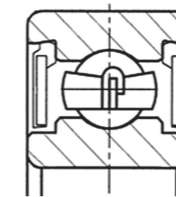


Radial contact

Axial contact

Consists of a structure where rubber seals are fitted in the outer ring. Since the rubber seal contacts the inner ring, there is very little intrusion of external contaminants. Mainly, NBR is used for the seal material. Limiting operating temperature range: -40 to +120°C. A fluoro rubber (FKM) type is also available for high temperatures. Limited operating temperature range: -30 to +230°C.

2RU: Non-contact rubber seals



Consists of a structure where rubber seals are fitted in the outer ring. The rubber seal does not contact the inner ring, and there is also less intrusion of external contaminants. There is less increase in torque, noise and temperature. Mainly, NBR is used for the seal material. Limiting operating temperature range: -40 to +120°C.

05 > Class, Tolerance and Chamfer Dimensions of Bearings

Tolerances of inner ring and outer ring width of radial ball bearings

Unit: μm

Nominal bore diameter d (mm)	Single plane mean bore diameter deviation Δ_{dmp}						Deviation of a single bore diameter Δ_{ds}		Bore diameter variation in single plane V_{dsp}								Mean bore diameter variation V_{dmp}					
	P0		P6	P5	P4	P4		P0		P6		P5		P4		P0	P6	P5	P4			
	Diameter series		Diameter series		Diameter series		Diameter series		Diameter series		P0	P6	P5	P4								
	0,1,2,3		7,8,9	0,1	2,3	7,8,9	0,1	2,3	7,8,9	0,1,2,3					7,8,9	0,1,2,3						
	Over	or less	Upper	Lower	Lower	Lower	Upper	Lower	Max.		Max.		Max.		Max.		Max.	Max.	Max.	Max.		
0.6(1)	2.5	0	-8	-7	-5	-4	0	-4	10	8	6	9	7	5	5	4	4	3	6	5	3	2
2.5	10	0	-8	-7	-5	-4	0	-4	10	8	6	9	7	5	5	4	4	3	6	5	3	2
10	18	0	-8	-7	-5	-4	0	-4	10	8	6	9	7	5	5	4	4	3	6	5	3	2
18	30	0	-10	-8	-6	-5	0	-5	13	10	8	10	8	6	6	5	5	4	8	6	3	2.5
30	50	0	-12	-10	-8	-6	0	-6	15	12	9	13	10	8	8	6	6	5	9	8	4	3
50	80	0	-15	-12	-9	-7	0	-7	19	19	11	15	15	9	9	7	7	5	11	9	5	3.5
80	120	0	-20	-15	-10	-8	0	-8	25	25	15	19	19	11	10	8	8	6	15	11	5	4
120	180	0	-25	-18	-13	-10	0	-10	31	31	19	23	23	14	13	10	10	8	19	14	7	5

Unit: μm

Nominal bore diameter d (mm)	Deviation of a single inner ring (or outer ring) width (2) Δ_{bs} (or Δ_{cs})				Inner ring (or outer ring) width variation (2) and variation of outer ring flange width (2) V_{bs} (or V_{cs}) and V_{cis}				Radial runout of assembled bearing inner ring K_{ia}				Perpendicularity of inner ring face with respect to the bore S_d		Assembled bearing inner ring face (back face) runout with raceway S_{ia}				
	Single bearing		Duplex bearing		Inner ring (or outer ring)		Inner ring		P0	P6	P5	P4	P5	P4	P5	P4			
	P0	P5	P0	P5	P0	P6	P5	P4											
	P6	P4	P6		P4														
	Over	or less	Upper	Lower	Lower	Upper	Lower	Lower	Max.	Max.	Max.	Max.	Max.	Max.	Max.	Max.	Max.		
0.6(1)	2.5	0	-40	-40	—	—	—	12	12	5	2.5	10	5	4	2.5	7	3	7	3
2.5	10	0	-120	-40	0	-250	-250	15	15	5	2.5	10	6	4	2.5	7	3	7	3
10	18	0	-120	-80	0	-250	-250	20	20	5	2.5	10	7	4	2.5	7	3	7	3
18	30	0	-120	-120	0	-250	-250	20	20	5	2.5	13	8	4	3	8	4	8	4
30	50	0	-120	-120	0	-250	-250	20	20	5	3	15	10	5	4	8	4	8	4
50	80	0	-150	-150	0	-380	-250	25	25	6	4	20	10	5	4	8	5	8	5
80	120	0	-200	-200	0	-380	-380	25	25	7	4	25	13	6	5	9	5	9	5
120	180	0	-250	-250	0	-500	-380	30	30	8	5	30	18	8	6	10	6	10	7

- Notes
- (1) 0.6 mm is included in this dimension classification.
 - (2) The deviation and variation of the outer ring width are determined based on the inner ring values of the same bearing. The variation of the outer ring width of P5 and P4 is obtained from the table "Tolerance of outer ring of radial ball bearings".

- Remarks
- The upper tolerance of the bearing bore diameter defined in this table is not applicable to the distance within 1.2 times the chamfer dimension r_{smax} from the ring face.
 - ABEC1, ABEC3, ABEC5 and ABEC7 of the inch series is equivalent to P0, P6, P5 and P4 of the metric series, respectively.
 - Please contact our company when the tolerance class is P2 or the tolerance is not indicated in the above table.

Tolerances of outer ring of radial ball bearings

Unit: μm

Nominal outside diameter D (mm)	Single plane mean bore diameter deviation Δ_{Dmp}				Deviation of a single outside diameter Δ_{Ds}		Outside diameter variation in a single radial plane (2) V_{Dsp}								Mean outside diameter variation (2) V_{Dmp}									
	P0		P6	P5	P4	P4		P0		P6		P5		P4		P0	P6	P5	P4					
	Open type		Sealed type		Open type		Sealed type		Open type		Open type													
	Diameter series		Diameter series		Diameter series		Diameter series		Diameter series		Diameter series		Diameter series											
	0,1,2,3		7,8,9	0,1	2,3	2,3	7,8,9	0,1	0,1,2,3	0,1,2,3	7,8,9	0,1,2,3	7,8,9	0,1,2,3										
Over	or less	Upper	Lower	Lower	Lower	Upper	Lower	Max.	Max.	Max.	Max.	Max.	Max.	Max.	Max.	Max.	Max.	Max.	Max.					
2.5(1)	6	0	-8	-7	-5	-4	0	-4	10	8	6	10	9	7	5	9	5	4	4	3	6	5	3	2
6	18	0	-8	-7	-5	-4	0	-4	10	8	6	10	9	7	5	9	5	4	4	3	6	5	3	2
18	30	0	-9	-8	-6	-5	0	-5	12	9	7	12	10	8	6	10	6	5	5	4	7	6	3	2.5
30	50	0	-11	-9	-7	-6	0	-6	14	11	8	16	11	9	7	13	7	5	6	5	8	7	4	3
50	80	0	-13	-11	-9	-7	0	-7	16	13	10	20	14	11	8	16	9	7	7	5	10	8	5	3.5
80	120	0	-15	-13	-10	-8	0	-8	19	19	11	26	16	16	10	20	10	8	8	6	11	10	5	4
120	150	0	-18	-15	-11	-9	0	-9	23	23	14	30	19	19	11	25	11	8	9	7	14	11	6	5
150	180	0	-25	-18	-13	-10	0	-10	31	31	19	38	23	23	14	30	13	10	10	8	19	14	7	5

Unit: μm

Nominal outside diameter D (mm)	Radial runout of assembled bearing outer ring K_{ea}				Perpendicularity of outer ring outside surface with respect to the face S_D		Assembled bearing outer ring face (back face) runout with raceway S_{ea}		Axial runout of outer ring flange back face of assembled bearing S_{eal}		Outer ring width variation (3) and variation of outer ring flange width (3) V_{cs} V_{cis}		
	P0		P6		P5		P4		P5		P4		
	Max.		Max.		Max.		Max.		Max.		Max.		
	P0		P6		P5		P4		P5		P4		
	Over	or less	Max.	Max.	Max.	Max.	Max.	Max.	Max.	Max.	Max.	Max.	
2.5(1)	6	15	8	5	3	8	4	8	5	11	7	5	2.5
6	18	15	8	5	3	8	4	8	5	11	7	5	2.5
18	30	15	9	6	4	8	4	8	5	11	7	5	2.5
30	50	20	10	7	5	8	4	8	5	11	7	5	2.5
50	80	25	13	8	5	8	4	10	5	14	7	6	3
80	120	35	18	10	6	9	5	11	6	16	8	8	4
120	150	40	20	11	7	10	5	13	7	18	10	8	5
150	180	45	23	13	8	10	5	14	8	20	11	8	5

- Notes
- (1) 2.5 mm is included in this dimension classification.
 - This is applicable when the snap ring is not mounted.
 - The width variation of the outer ring of P0 and P6 is based on the tolerance of the inner ring.

- Remarks
- The lower tolerance of the bearing outside diameter defined in this table is not applicable to the distance within 1.2 times the chamfer dimension r_{smax} from the ring face.
 - ABEC1, ABEC3, ABEC5 and ABEC7 of the inch series is equivalent to P0, P6, P5 and P4 of the metric series, respectively.
 - Please contact our company when the tolerance class is P2 or the tolerance is not indicated in the above table.

Technical Contents

05 Class, Tolerance and Chamfer Dimensions of Bearings

Unit: μm

Nominal flange outside diameter D1 (mm)		Deviation of a single outside diameter of outer ring flange Δ_{D1s}			
		P0 P6		P5 P4	
Over	or less	Upper	Lower	Upper	Lower
2.5 (1)	6	125	-50	0	-25
6	18	125	-50	0	-25
18	30	125	-50	0	-52
30	50	125	-50	0	-62
50	80	460	-74	0	-74
80	120	540	-87	0	-87
120	150	630	-100	0	-100
150	180	630	-100	0	-100

Notes

(1) 2.5 mm is included in this dimension classification.

Remarks

- The lower tolerance of the bearing outside diameter defined in this table is not applicable to the distance within 1.2 times the chamfer dimension r_{smax} from the the ring face.
- ABEC1, ABEC3, ABEC5 and ABEC7 of the inch series is equivalent to P0, P6, P5 and P4 of the metric series, respectively.
- Please contact our company when the tolerance class is P2 or the tolerance is not indicated in the above table.

Tolerances of inner ring and outer ring width of radial ball bearings (high-precision instrument ball bearings)

 Unit: μm

Nominal bore diameter d (mm)		Single plane mean bore diameter deviation Δ_{dmp}	Deviation of a single bore diameter Δ_{ds}		Bore diameter variation in single plane V_{dsp}		Mean bore diameter variation V_{dmp}	Deviation of a single inner ring width Δ_{Bs}		Inner ring width variation Δ_{Bs}		Radial runout of assembled bearing inner ring K_{ia}		Assembled bearing inner ring face (back face) runout with raceway S_{ia}		Perpendicularity of inner ring face with respect to the bore S_d	
			Upper	Lower	Max.	Max.		Upper	Lower	Max.	Max.	Max.	Max.	Max.	Max.	Max.	Max.
—	10	0	-5.1	0	-5.1	2.5	2.5	0	-25.4	5.1	2.5	3.8	2.5	7.6	2.5	7.6	2.5
10	18	0	-5.1	0	-5.1	2.5	2.5	0	-25.4	5.1	2.5	3.8	2.5	7.6	2.5	7.6	2.5
18	30	0	-5.1	0	-5.1	2.5	2.5	0	-25.4	5.1	2.5	3.8	3.8	7.6	3.8	7.6	3.8

 Unit: μm

Nominal bore diameter d (mm)		Deviation of a single outer ring flange width Δ_{C1s}	
		P0 P6	P5 P4
Over	or less	Upper	Lower
0.6 (1)	2.5	0	-50
2.5	10	0	-50
10	18	0	-50
18	30	0	-50
30	50	0	-120
50	80	0	-150
80	120	0	-200
120	150	0	-250

Tolerances of outer ring of radial ball bearings (high-precision instrument ball bearings)

 Unit: μm

Nominal outer diameter D (mm)		Single plane mean bore diameter deviation Δ_{Dmp}	Deviation of a single outside diameter Δ_{Ds}				Outside diameter variation in a single radial plane (2) V_{Dsp}		Mean outside diameter variation (2) V_{Dmp}		Deviation of a single outer ring width Δ_{Cs}		Outer ring width variation (1) V_{Cs}		Perpendicularity of outer ring outside surface with respect to the face S_0		Radial runout of assembled bearing outer ring K_{ea}		Assembled bearing outer ring face (back face) runout with raceway S_{ea}		
			ABEC5P ABEC7P		Open type		Sealed type		ABEC5P ABEC7P		ABEC5P ABEC7P		ABEC5P ABEC7P		ABEC 5P	ABEC 7P	ABEC 5P	ABEC 7P	ABEC 5P	ABEC 7P	
Over	or less	Upper	Lower	Upper	Lower	Upper	Lower	Max.	Max.	Max.	Max.	Upper	Lower	Max.	Max.	Max.	Max.	Max.	Max.	Max.	
—	18	0	-5.1	0	-5.1	+1.0	-6.1	2.5	5.1	2.5	5.1	0	-25.4	5.1	2.5	7.6	3.8	5.1	3.8	7.6	5.1
18	30	0	-5.1	0	-5.1	+1.0	-6.1	2.5	5.1	2.5	5.1	0	-25.4	5.1	2.5	7.6	3.8	5.1	3.8	7.6	5.1
30	50	0	-5.1	0	-5.1	+1.0	-6.1	2.5	5.1	2.5	5.1	0	-25.4	5.1	2.5	7.6	3.8	5.1	5.1	7.6	5.1

 Unit: μm

Nominal outside outer D (mm)		Deviation of a single outside diameter of outer ring flange Δ_{D1s}		Deviation of a single outer ring flange width Δ_{C1s}		Variation of outer ring flange width V_{C1s}		Axial runout of outer ring flange back face of assembled bearing S_{a1}
		ABEC5P ABEC7P		ABEC5P ABEC7P		ABEC5P ABEC7P		ABEC5P ABEC7P
Over	or less	Upper	Lower	Upper	Lower	Max.	Max.	Max.
—	18	0	-25.4	0	-50.8	5.1	2.5	7.6
18	30	0	-25.4	0	-50.8	5.1	2.5	7.6
30	50	0	-25.4	0	-50.8	5.1	2.5	7.6

Notes

(1) This is also applicable to the flange width variation of a flanged bearing.

Remarks

- ABEC5P and ABEC7P is the tolerance and class of high-precision instrument ball bearings.
- Please contact our company when the tolerance class is ABEC9P or the tolerance is not indicated in the above table.

Tolerances of thrust ball bearings

● Tolerances of shaft washer (inner ring)

Unit: μm

Class	Nominal bore diameter d (mm)		Single plane mean bore diameter deviation Δ_{dmp}		Bore diameter variation in single plane V_{dsp}	Raceway to back face thickness variation of shaft washer (inner ring) S_i
	Over	or less	Upper	Lower	Max.	Max.
P0	—	18	0	-8	6	10
	18	30	0	-10	8	10
	30	50	0	-12	9	10
P6	—	18	0	-8	6	5
	18	30	0	-10	8	5
	30	50	0	-12	9	6
P5	—	18	0	-8	6	3
	18	30	0	-10	8	3
	30	50	0	-12	9	3
P4	—	18	0	-7	5	2
	18	30	0	-8	6	2
	30	50	0	-10	8	2

● Tolerances of housing washer (outer ring)

Unit: μm

Class	Nominal outer diameter D (mm)		Single plane mean bore diameter deviation Δ_{Dmp}		Outside diameter variation in a single radial plane (2) V_{Dsp}	Raceway to back face thickness variation of housing washer (outer ring) S_e
	Over	or less	Upper	Lower	Max.	Max.
P0	—	18	0	-11	8	Same as the value of S_i for d of the same bearing
	18	30	0	-13	10	
	30	50	0	-16	12	
P6	—	18	0	-11	8	
	18	30	0	-13	10	
	30	50	0	-16	12	
P5	—	18	0	-11	8	
	18	30	0	-13	10	
	30	50	0	-16	12	
P4	—	18	0	-7	5	
	18	30	0	-8	6	
	30	50	0	-9	7	

● Tolerance of bearing height

Unit: μm

Class	Nominal bore diameter d (mm)		Deviation of the actual bearing height Δ_{Tg}	
	Over	or less	Upper	Lower
P0, P6, P5, P4	—	50	+20	-250

Selection Criteria of Tolerance

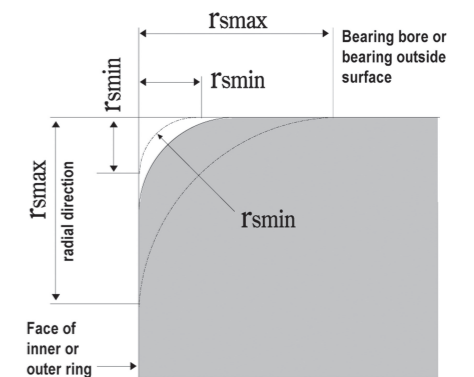
Required Function	Application Examples	Tolerance Class
General precision	Small-size motors, gear mechanisms, cam mechanisms, generators, stepper motor, pinch rollers, printers, copy mechanisms and measuring instruments	P0, P6, ABEC1, ABEC3
Low torque and slight torque fluctuation	High frequency spindles, servomotors, potentiometers, gyroscope gimbals	P4, ABEC7P
High-speed operation	Turbochargers, centrifugal separators, dental drill spindles, high frequency spindles, tension reels	P5, P4, ABEC5P, ABEC7P
High rotational accuracy	Hard disk motors, encoders, polygon mirror motors, synchronous motors, machine tool spindles	P5, P4, ABEC5P, ABEC7P
Corrosion resistance	Dental drill spindles, surgery assist robots, in vitro fertilization device, peristalsis pumps	P5, P4, ABEC5P, ABEC7P
	Food processors, food and beverage filling machines, electric adjustable beds, robot suits for nursing care	P0, P6, ABEC1, ABEC3

Chamfer Dimensions Limits for Radial Bearings

Permissible chamfer dimensions of inner/outer rings r_{min}	Nominal bore diameter d (mm)		Permissible chamfer dimensions of inner/outer rings r_{max}		(Reference) Radius of rounded corners of shafts or housings r_{max}
	Over	or less	Radial direction	Axial direction	
0.05	—	—	0.1	0.2	0.05
0.08	—	—	0.16	0.3	0.08
0.1	—	—	0.2	0.4	0.1
0.15	—	—	0.3	0.6	0.15
0.2	—	—	0.5	0.8	0.2
0.25	—	—	0.55	0.9	0.25
0.3	—	40	0.6	1	0.3
	40	—	0.8	1	
0.4	—	—	0.7	1.1	0.4
0.5	—	—	0.9	1.2	0.5
0.6	—	40	1	2	0.6
	40	—	1.3	2	
0.8	—	—	1.2	2.2	0.8
1	—	50	1.5	3	1
	50	—	1.9	3	
1.1	—	120	2	3.5	1
	120	—	2.5	4	
1.5	—	120	2.3	4	1.5
	120	—	3	5	

Chamfer Dimensions Limits for Thrust Bearings

Permissible chamfer dimensions of inner/outer rings r_{min}	Permissible chamfer dimensions of inner/outer rings r_{max}	(Reference) Radius of rounded corners of shafts or housings r_{max}
	Radial direction and axial direction	
0.05	0.1	0.05
0.08	0.16	0.08
0.1	0.2	0.1
0.15	0.3	0.15
0.2	0.5	0.2
0.3	0.8	0.3
0.6	1.5	0.6
1	2.2	1
1.1	2.7	1.1



rs: Chamfer dimension of inner/outer rings

Remarks

- There are no regulations for the accurate shape of the chamfered surface. However, the profile in the axial plane must not extend outside the virtual arc of the radius r_{min} which contacts the face of the inner ring and bearing bore, or the face of the outer ring and bearing outside diameter.

06 > Life and Load Rating

Bearing Life

- The raceway and raceway surface of the inner/outer rings of the bearing continuously receive a repeated load, when rotated with a load applied. This causes material fatigue that results in a damage called flaking. The total rotational frequency to this point is called rolling fatigue life.
- The life of a bearing is based on a statistical value because there is a considerably large variation even though the same dimensions, material and heat treatment processing method are used to operate the bearing under the same conditions. Therefore, generally, the total rotating speed in which 90% of the bearings can be operated without the occurrence of flaking is called the basic rating life.

Basic Dynamic Load Rating

The basic dynamic load rating is the constant load applied in a direction under which the basic rating life of the bearing reaches 1 million revolutions. This is the centric radial load in radial bearings, and the centric axial load in thrust bearings. Also, for duplex bearings that consist of two single-row radial bearings with adjusted standouts, the basic dynamic load rating is converted by about 1.62 times that of a single-row bearing.

Life Equation

The relationships between the basic dynamic load rating, dynamic equivalent load, and the basic rating life of ball bearings are as follows.

Total rotating speed	$L_{10} = (C/P)^3 \times 10^6$ (Revolutions)
Operating hours	$L_{10h} = (C/P)^3 \times 16667/n$ (hours)
Distance	$L_{10d} = \pi \times D \times L_{10} \times 10^{-6}$ (km)
Minimum basic dynamic load rating for operating conditions	$C_{min} = P \times (L_{10h} \times n / 16667)^{1/3}$ (N)

L_{10h} can be obtained by the following equation using life factor (f_h) and speed factor (f_n).

$$L_{10h} = 500 \times f_n^3, f_h = f_n \times C/P, f_n = (33.3/n)^{1/3}$$

- L_{10} =basic rating life (rev)
- L_{10h} =basic rating life (h)
- L_{10d} =basic rating life (km)
- P =dynamic equivalent load (N)
 - ※ Expressed as P_r in radial bearings and P_a in thrust bearings
- C =basic dynamic load rating (N)
 - ※ Expressed as C_r in radial bearings and C_a in thrust bearings
- C_{min} =minimum basic dynamic load rating (N)
- n =rotating speed (min^{-1})
- D =rotating body outside diameter dimension (mm)

● How to select basic rating life L_{10h}

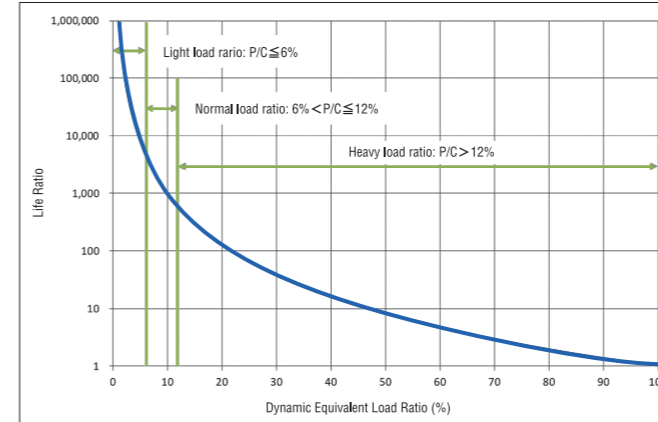
Operating Conditions of a Machine	Basic rating life (h) L_{10h}
In the case of low frequency of use	500
In the case of no great effect when a machine used for a short time or intermittently fails	4,000~8,000
In the case of great effect when a machine used intermittently fails	8,000~12,000
When a machine is used for 8 hours per day without being in full operation at all times	12,000~20,000
When a machine is operated full time 8 hours per day	20,000~30,000
When a machine is continuously operated 24 hours per day	40,000~60,000
When a machine is continuously operated 24 hours per day, and absolutely no stoppage due to failure is allowed	100,000~200,000

Selection method of bearings in consideration of life for the operating conditions

When a large dynamic equivalent load P close to the basic dynamic load rating C is applied to a bearing, the bearing life is reduced in a very short time. However, when a bearing rotates at a high speed with high acceleration, or beyond the limiting speed $\times 0.5$, it is necessary to set to $P/C \geq 1\%$ in general, in order to prevent the occurrence of damage due to the sliding of the balls and the raceway surface.

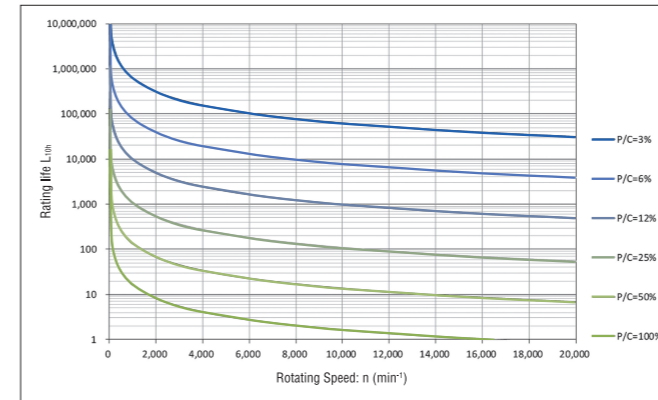
A suitable bearing type must be selected based on $C_{min} = P \times (L_{10h} \times n / 16667)^{1/3}$ by clarifying the operating conditions of the machine (dynamic equivalent load P , rotating speed n) and the required lifetime L_{10h} in advance.

As shown in the following table and graph, generally, it is necessary to consider selection of a bearing using [dynamic equivalent load] / [dynamic load rating] = P/C = [normal load ratio: 6 to 12%] as a guide.



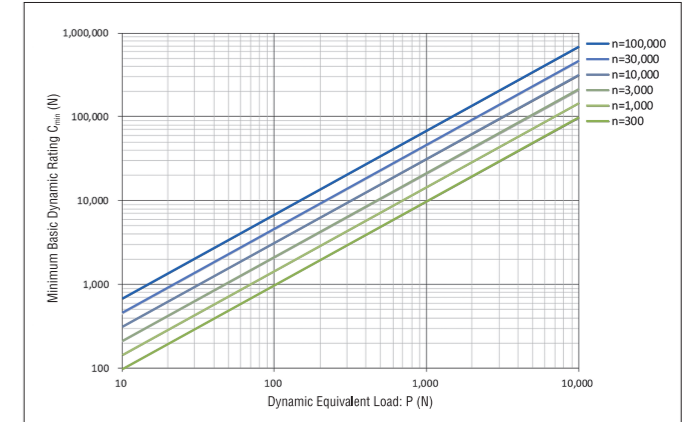
Dynamic Equivalent Load Ratio: P/C and Life Ratio

When P/C and n are known, rating life: L_{10h} can be obtained easily using the following graph.



Dynamic Equivalent Load Ratio: P/C , Rotating Speed: n and Rating life: L_{10h}

If P and n are known based on $L_{10h} = 50,000$ hours as a reference, the minimum basic dynamic load rating: C_{min} can be obtained easily using the upper right graph. It is recommended to select a bearing type with a basic dynamic load rating: C higher than this C_{min} . However, rotating speed: n must not exceed the limiting speed of the selected bearing type.



Dynamic Equivalent Load: P , Rotating Speed: n and Minimum Basic Dynamic Load Rating: C_{min}

Modification of Life Equation

Generally, the life can be calculated by the above equation, however, it is insufficient when a high reliability of 90% or more is required depending on the application. Since the fatigue life of bearings has been prolonged due to improved bearing steel in recent years, and the relationship between the lubricant and the bearing life has also been clarified, the following modified life equation is used in ISO281.

$$L_{na} = a_1 \times a_2 \times a_3 \times L_{10}$$

L_{na} : Modified rating life [life when the level of reliability is based (100— n) %]

L_{10} : Basic rating life (rev)

a_1 : Life modification factor for reliability

a_2 : Life modification factor for bearing characteristics

a_3 : Life modification factor for operating conditions

(1) Life modification factor for reliability a_1

When calculating the life with a reliability of 90% or more, modify the value according to the following factor a_1 .

● Values of life modification factor for reliability a_1

Reliability (%)	90	95	96	97	98	99	99.2	99.4	99.6	99.8	99.9	99.92	99.94	99.95
Reliability Factor a_1	1	0.64	0.55	0.47	0.37	0.25	0.22	0.19	0.16	0.12	0.093	0.087	0.08	0.077

(2) Life modification factor for bearing characteristics a_2

When the fatigue life is prolonged due to improvements in the manufacturing method and heat treatment condition, etc. of the bearing material, modify the value according to the life modification factor for bearing characteristics a_2 . In the case of the standard bearing material of our company, modify the value to $a_2=1$.

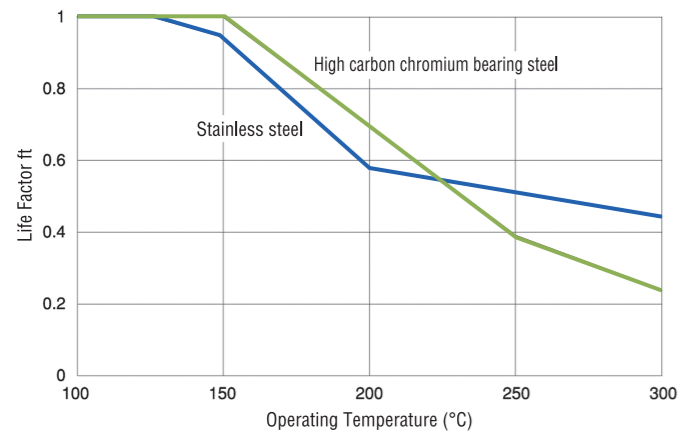
(3) Life modification factor for operating conditions a_3

In the operating conditions of a bearing, the modification factors which originate in the conditions of the lubrication, temperature and load, etc. is called "the life modification factor for operating conditions a_3 ". In the case of favorable lubrication conditions, where there is no metal contact due to a lubricating film applied between the raceway surface and balls, and dynamic viscosity of lubricant is above 13 mm²/s (13cSt), then $a_3=1$ is used for the effect of the lubrication on the life.

When the operating conditions are not favorable ($d_{mn} \leq 10,000$, deterioration of lubricant, large inclination of inner/outer rings), $a_3 < 1$ is used. If the operating temperature exceeds 120°C, the life becomes shorter because the dimensional change becomes larger, and also the hardness deteriorates. The operating temperature and the life modification factor in such a case are based on the following table.

Remarks: d_{mn} is the rolling element pitch circle diameter (mm) x rotating speed (min⁻¹).

● Value of temperature factor f_t



● Dimensional Stabilization Treatment

Dimensional stabilization treatment symbol	S0	S1	S2	S3
Maximum operating temperature (°C)	150	200	250	300

※ The dimensional change of a bearing with normal heat treatment applied becomes larger at temperatures exceeding 120°C. Although a reduction in the basic dynamic load rating due to the deterioration of the hardness is unavoidable, the dimensional change can be suppressed even at high temperatures by performing a dimensional stabilization treatment.

System Life of Multiple Bearings

The basic rating life of each bearing has a probability of 90%. The system life of multiple bearings becomes even shorter than the shortest basic rating life of each bearing. Considering all the bearings being used as one bearing system, the system life can be obtained by the following equation.

$$L = \frac{1}{\left(\frac{1}{L_1^{10/9}} + \frac{1}{L_2^{10/9}} + \dots + \frac{1}{L_n^{10/9}}\right)^{9/10}}$$

L =rating life of entire bearing system
 $L_1, L_2, L_3, \dots, L_n$ =rating life of each bearing

Basic Static Load Rating

When a certain static load is applied to a bearing, a local permanent deformation of an indent shape occurs in the contact portion between the balls and raceway surface. This permanent deformation causes a poor rotating condition that also increases noise and vibrations, therefore, the basic static load rating C_0 is defined as follows as a reference of the acceptable static load. The basic static load rating of a ball bearing is the static load where the calculated contact stress becomes 4200 MPa (429kgf/mm²) in the contact portion between the balls and raceway, and the sum of the permanent deformation produced between the balls and raceway becomes about 1/10000 of the ball diameter. The value of the basic static load rating C_0 is expressed as C_{or} for radial bearings and C_{0a} for thrust bearings. In addition, the C_0 of duplex bearings that consist of two single-row radial bearings with adjusted standouts is converted by twice that of a single-row bearing.

Calculation of Bearing Load

The loads applied to the bearings include drive loads, such as belts and gears, loads that occur in a machine during operation, and the self-weight of equipment supported by bearings. When a bearing is used, it is difficult to obtain the entire load accurately as the bearing load, because different levels of vibration and impact loads are applied. Normally, the load is obtained by multiplying the various factors based on the experience acquired conventionally with the calculated load value obtained theoretically.

(1) Load factor, gear factor and belt factor

The radial load and axial load applied to a bearing can be obtained by a theoretical calculation. However, the actually applied load becomes larger than the calculated value due to the vibration and impact of the equipment, therefore the load is obtained by multiplying the factors as follows.

Gear drive	$F = f_w \cdot f_g \cdot F_c$
Belt and chain drive	$F = f_w \cdot f_b \cdot F_c$

F : actually applied load (N)
 F_c : theoretically calculated load (N)
 f_w : load factor
 f_g : gear factor
 f_b : belt factor

● Load factor f_w

Operating Conditions	Examples	f_w
No impact	Motors, machine tools, meters, conveyors	1~1.2
Light impact	Fans, cranes, compressors, pumps, elevators, paper-making machines	1.2~1.5
Strong impact	Rolling mills, crushers, drop hammers, vibrating filters	1.5~3

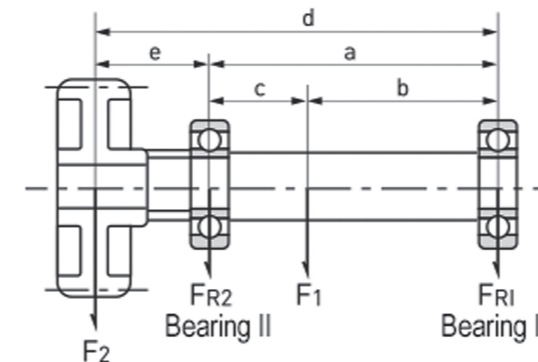
● Gear factor f_g

Type of Gears	f_g
Precision gears [Pitch error ≤ 0.02 mm, shape error ≤ 0.02 mm]	1.0~1.1
Ordinary gears [Pitch error ≤ 0.1 mm, shape error ≤ 0.1 mm]	1.1~1.3

● Belt factor f_b

Type of Belts	f_b
Flat belts (without tension pulley)	4.0~5.0
Flat belts (with tension pulley)	2.5~3.0
V-belts	2.0~2.5
Toothed belts	1.3~2.0
Chains	1.2~1.5

(2) Load distribution on bearings



As shown in the figure, when radial loads F_1 and F_2 are applied, the load distributed on Bearing I and Bearing II can be obtained by the following equation.

$$F_{R1} = c/a \times F_1 - e/a \times F_2$$

$$F_{R2} = b/a \times F_1 + d/a \times F_2$$

(3) Average load of fluctuating load

When the scale and direction of the load applied to a bearing fluctuates, it is necessary to obtain the average load so that it becomes equal to the bearing life under its loading condition.

Load Patterns	$P_m = A P_2 + B P_1$						
	P_1/P_2	0	0.2	0.4	0.6	0.8	1.0
1. Circular and elliptical shapes 	A	0.84	0.83	0.82	0.81	0.79	0.78
	B	0.16	0.17	0.18	0.19	0.21	0.22
2. Sine and cosine shapes 	A	0.75	0.73	0.70	0.68	0.66	0.64
	B	0.25	0.27	0.30	0.32	0.34	0.36
3. Sine and cosine shapes 	A	0.68	0.64	0.60	0.56	0.53	0.50
	B	0.32	0.36	0.40	0.44	0.47	0.50
4. Linear 	A	0.63	0.60	0.57	0.54	0.52	0.50
	B	0.37	0.40	0.43	0.46	0.48	0.50
5. Sine and cosine shapes 	A	0.56	0.50	0.45	0.42	0.38	0.36
	B	0.44	0.50	0.55	0.58	0.62	0.64
6. Circular and elliptical shapes 	A	0.38	0.32	0.27	0.25	0.23	0.22
	B	0.62	0.68	0.73	0.75	0.77	0.78
7. Gradual fluctuations 	$P_m = \sqrt[3]{\frac{P_1^3 n_1 t_1 + P_2^3 n_2 t_2 + \dots + P_n^3 n_n t_n}{n_1 t_1 + n_2 t_2 + \dots + n_n t_n}}$ $n_m = \frac{n_1 t_1 + n_2 t_2 + \dots + n_n t_n}{t_1 + t_2 + \dots + t_n}$						
8. Active state of static load and rotational load at the same time P1: Rotational load P2: Static load (P2 > P1) 	$P_m = \frac{P_1^2 + P_1 P_2 + P_2^2}{P_1 + P_2}$						
9. Oscillating load θ_0 : Minimum critical oscillating angle θ : Actual oscillating angle ($\theta > \theta_0$) 	$P_m = \left(\frac{\theta}{180}\right)^{1/3} \cdot P$ <p>(Note: $\theta \geq \theta_0 = \frac{200}{Z}$) (Z = number of balls)</p>						

Dynamic Equivalent Load

Although the load condition is not constant when a bearing is actually used, there are many cases where the load is a combination of the radial load and axial load. In such a case, it is necessary to calculate the load so that the direction and scale become constant. The calculated virtual load is called dynamic equivalent load P, and is expressed as P_r for radial bearings and P_a for thrust bearings.

(1) Radial bearings

Bearing Types	Axial Load Ratio	Single-Row Bearings				Double-Row Bearings				e	
		$\frac{F_a}{F_r} \leq e$		$\frac{F_a}{F_r} > e$		$\frac{F_a}{F_r} \leq e$		$\frac{F_a}{F_r} > e$			
		X	Y	X	Y	X	Y	X	Y		
Deep groove ball bearings	$\frac{F_a}{iZD_w^2}$										
	0.172				2.3				2.3	0.19	
	0.345				1.99				1.99	0.22	
	0.689				1.71				1.71	0.26	
	1.03	1	0	0.56	1.55	1	0	0.56	1.55	0.28	
	1.38				1.45				1.45	0.3	
	2.07				1.31				1.31	0.34	
	3.45				1.15				1.15	0.38	
	5.17				1.04				1.04	0.42	
	6.89				1				1	0.44	
Angular contact ball bearings	$\frac{F_a}{ZD_w^2}$									Single-row bearings	Double-row bearings
	0.172				2.3		2.78		3.74	0.19	0.23
	0.345				1.99		2.4		3.23	0.22	0.26
	0.689				1.71		2.07		2.78	0.26	0.3
	1.03	1	0	0.56	1.55	1	1.87	0.78	2.52	0.28	0.34
	1.38				1.45		1.75		2.36	0.3	0.36
	2.07				1.31		1.58		2.13	0.34	0.4
	3.45				1.15		1.39		1.87	0.38	0.45
	5.17				1.04		1.26		1.69	0.42	0.5
	6.89				1		1.21		1.63	0.44	0.52
	0.172				1.88		2.18		3.06	0.29	
	0.345				1.71		1.98		2.78	0.32	
	0.689				1.52		1.76		2.47	0.36	
	1.03				1.41		1.63		2.29	0.38	
	1.38	1	0	0.46	1.34	1	1.55	0.75	2.18	0.4	
	2.07				1.23		1.42		2	0.44	
	3.45				1.1		1.27		1.79	0.49	
	5.17				1.01		1.17		1.64	0.54	
	6.89				1		1.16		1.63	0.54	
	0.172				1.47		1.65		2.39	0.38	
0.345				1.4		1.57		2.28	0.4		
0.689				1.3		1.46		2.11	0.43		
1.03				1.23		1.38		2	0.46		
1.38	1	0	0.44	1.19	1	1.34	0.72	1.93	0.47		
2.07				1.12		1.26		1.82	0.5		
3.45				1.02		1.14		1.66	0.55		
5.17				1		1.12		1.63	0.56		
6.89				1		1.12		1.63	0.56		
a=20°	—			0.43	1	1.09	0.7	1.63	0.57		
a=25°	—			0.41	0.87	0.92	0.67	1.41	0.68		
a=30°	—			0.39	0.76	0.78	0.63	1.24	0.8		
a=35°	—	1	0	0.37	0.66	0.66	0.6	1.07	0.95		
a=40°	—			0.35	0.57	0.55	0.57	0.93	1.14		
a=45°	—			0.33	0.5	0.47	0.54	0.81	1.34		

Dynamic equivalent radial load P_r of a radial bearing is expressed by the following equation.

$$P_r = X \times F_r + Y \times F_a$$

P_r =dynamic equivalent radial load (N) X =radial load factor
 F_r =radial load (N) Y =axial load factor
 F_a =axial load (N) D_w =ball diameter (mm)
 i =number of rows of balls Z =number of balls per row

(2) Thrust bearings

Dynamic equivalent axial load P_a of a thrust bearing is expressed by the following equation.

$$P_a = F_a \text{ (when } \alpha = 90^\circ \text{)}$$

※ Contact angle α of our thrust bearing is 90° .

Static Equivalent Load

The virtual load of the combination of the radial load and axial load that is received when the bearing is static (including very low speed rotations) which is calculated to ensure that the direction and scale become constant is called static equivalent load P_0 and is expressed as P_{0r} for radial bearings and P_{0a} for thrust bearings.

The higher value of static equivalent radial load P_{0r} of a radial bearing is used among the values calculated by the following two equations.

$$P_{0r} = 0.6 \times F_r + 0.5 \times F_a, \quad P_{0r} = F_r$$

Static equivalent axial load P_{0a} of a thrust bearing is expressed by the following equation.

$$P_{0a} = F_a \text{ (when } \alpha = 90^\circ \text{)}$$

※ Contact angle α of our thrust bearing is 90° .

Safety Factor

The acceptable static equivalent load of a bearing is determined by the basic static load rating, however, the usage limitations of a bearing differ by the operating conditions and required performance. Therefore, in order to examine the safety integrity, the value can be calculated by the following equation using an experiential safety factor.

$f_s = C_0 / P_0$ f_s =safety factor
 C_0 =basic static load rating (N)
 P_0 =static equivalent load (N)

Operating Conditions	f_s (min)
Normal operating conditions	1.0
Impact load	1.5
Quiet and high precision rotation is required	2.0

Applied Calculation for Life and Load

● Calculation Example 1

Assuming that the bearing bore diameter ≤ 10 mm, outside diameter ≤ 20 mm, and width ≤ 5 mm are for the space to assemble a bearing, and the load condition is F_r (radial load) = 120 N and rotating speed $n = 1200 \text{ min}^{-1}$, select the type of single-row deep groove ball bearing with a life factor $f_h \geq 4$.

Obtain speed factor f_n as follows

$$f_n = \left(\frac{33.3}{n} \right)^{1/3} = \left(\frac{33.3}{1200} \right)^{1/3} = 0.303$$

If C_r is obtained from the equation $(f_h = f_n \times \frac{C_r}{P})$, the following equation holds:

$$C_r = \frac{f_h}{f_n} \times P = \frac{4}{0.303} \times 120 = 1584 \text{ N}$$

Bearings with such a basic dynamic load rating selected from the dimensions table are as shown in the table below:

Part No.	Bore Diameter (mm)	Outside Diameter (mm)	Width (mm)	Basic Dynamic Load Rating (N)
625	5	16	5	1730
697	7	17	5	1610
6800	10	19	5	1720

● Calculation Example 2

Select the bearing that has the smallest bore diameter, when selection conditions for the bearing are as follows: Material: SUJ2, Deep groove ball bearing: 60 series, Required life time: 10,000 hours or more, Radial load $F_r=150$ N, Axial load $F_a=20$ N, Rotating speed $n = 5000 \text{ min}^{-1}$.

Calculate P_r (the temporary dynamic equivalent radial load) as follows:

$$\frac{F_a}{F_r} = \frac{20}{150} = 0.13$$

Since this is smaller than any "e" value in the table, the following equation can be considered: $P_r = F_r = 150$ N.

Obtain C_{min} (the minimum basic dynamic load rating for operating conditions) as follows:

$$C_{min} = P_r \times \left(L_{10} \times \frac{n}{16667} \right)^{1/3}$$

$$= 150 \times \left(10000 \times \frac{5000}{16667} \right)^{1/3} = 2163 \text{ N}$$

The bearing number with the smallest bore diameter whose C_r is 2163N or higher and the material is SUJ2 in the 60 series will be 606.

Calculate the value of P_r (dynamic equivalent radial load of 606), and check that the P_r obtained first (temporary dynamic equivalent radial load) is correct.

The axial load ratio of 606 is as follows:

$$\frac{F_a}{iZD_w^2} = \frac{20}{1 \times 6 \times 3.5^2} = 0.272$$

From above, the following equation is obtained:

$$e = \frac{0.272 - 0.172}{0.345 - 0.172} \times (0.22 - 0.19) + 0.19 = 0.207$$

Thus, from

$$\frac{F_a}{F_r} = 0.13 < e, \text{ the equation } P_r = F_r = 150 \text{ N}$$

is derived, which indicates that the temporary dynamic equivalent radial load obtained first is correct.

● Calculation Example 3

What is the average radial load when the following variable radial load is applied?

$P_1 = 300 \text{ N}, n_1 = 1800 \text{ min}^{-1}, t_1 = 10 \text{ (s)}$
 $P_2 = 100 \text{ N}, n_2 = 3000 \text{ min}^{-1}, t_2 = 15 \text{ (s)}$
 $P_3 = 200 \text{ N}, n_3 = 1000 \text{ min}^{-1}, t_3 = 20 \text{ (s)}$

Obtain P_m from Eq. (3) 7 of "Gradual fluctuations":

$$P_m = \sqrt[3]{\frac{300^3 \times 1800 \times 10 + 100^3 \times 3000 \times 15 + 200^3 \times 1000 \times 20}{1800 \times 10 + 3000 \times 15 + 1000 \times 20}}$$

$$\approx 203 \text{ N}$$

● **Calculation Example 4**

What is the system life when the following radial rotational load and radial static load are applied to 6000HZZ, 6202HZZ and 6304HZZ?

Part No.	Radial Rotational Load (N)	Radial Static Load (N)
6000HZZ	100	250
6202HZZ	200	400
6304HZZ	500	800

Obtain P_m from Eq. (3) 8 of "Active state of static load and rotational load at the same time," and L_{10} from the equation for "Life equation (operating hours)":

In the case of 6000HZZ:

$$P_m = \frac{100^2 + 100 \times 250 + 250^2}{100 + 250} = 279 \text{ N}$$

As C_r of 6000HZZ is 3890N, the following equation holds:

$$L_{10} = \left(\frac{3890}{279} \right)^3 \times 10^6 = 2710 \times 10^6 \text{ rotations}$$

L_{10} for the following also can be obtained in the same way:

Part No.	P_m (N)	C_r (N)	L_{10} (rotation)
6202HZZ	467	6490	2684×10^6
6304HZZ	992	13500	2520×10^6

Thus, the following is obtained from the equation for the system life of multiple bearings

$$L = \frac{1}{\left(\frac{1}{(2710 \times 10^6)^{10/9}} + \frac{1}{(2684 \times 10^6)^{10/9}} + \frac{1}{(2520 \times 10^6)^{10/9}} \right)^{9/10}}$$

$$= 980.4 \times 10^6 \text{ rotations}$$

● **Calculation Example 5**

What is the lifetime L_{10h} when radial load 150 N is applied to 688ZZ, and oscillates 1,000 time per minute at an oscillating angle of 30°?

688ZZ uses 10 ϕ 2-mm balls. C_r is 1260N.

$$\theta_0 \geq \frac{200}{10} = 20^\circ \dots \text{minimum critical oscillating angle}$$

Since $\theta = 30^\circ > \theta_0 = 20^\circ$, it can be used.

Obtain P_m from Eq. (3) 9 of "Oscillating load":

$$P_m = \left(\frac{30}{180} \right)^{1/3} \times 150 = 83 \text{ N}$$

L_{10h} is obtained from the equation for life equation (operating hours):

$$L_{10h} = \left(\frac{1260}{83} \right)^3 \times \frac{16667}{1000} = 58309 \text{ hours}$$

● **Calculation Example 6**

What is the life time L_{10h} , L_{1h} where a stainless steel deep groove ball bearing 6706H 2RU is continuously operated at Radial load $F_r = 100$ N, Axial load $F_a = 40$ N, Speed $n = 1800 \text{ min}^{-1}$? Also, what is the grease life when 6706H 2RU is continuously operated at a bearing temperature of 80°C under the same conditions?

For 6706H 2RU: $C_r = 969$ N, and $C_{or} = 757$ N

Ball used: $D_w = 1.588$ mm, $Z = 24$ balls

According to the table of Dynamic Equivalent Load (Radial Bearings - factors X and Y of deep groove ball bearings) in this section, it becomes:

$$\frac{F_a}{iZD_w^2} = \frac{40}{1 \times 24 \times 1.588^2} = 0.661$$

$$e = \frac{0.661 - 0.345}{0.689 - 0.345} \times (0.26 - 0.22) + 0.22 = 0.257$$

$$\frac{F_a}{F_r} = \frac{40}{100} = 0.4 > e = 0.257$$

$$\text{Therefore, } Y = \frac{0.661 - 0.345}{0.689 - 0.345} \times (1.71 - 1.99) + 1.99 = 1.733$$

According to $X = 0.56$, $Y = 1.733$ and the equation of dynamic equivalent radial load, the following equation holds:

$$P_r = 0.56 \times 100 + 1.733 \times 40 = 125 \text{ N}$$

Therefore, the following is obtained from the equation for life equation (operating hours):

$$L_{10h} = \left(\frac{969}{125} \right)^3 \times \frac{16667}{1800} = 4313 \text{ hours}$$

L_{1h} can also be obtained as follows according to the reliability factor $a_1 = 0.25$ when the reliability is 99%:

$$L_{1h} = 0.25 \times L_{10h} = 0.25 \times 4313 = 1078 \text{ hours}$$

When general purpose grease is applied, the grease life can be obtained according to Eq. (8) of "09. Lubrication":

$$\log L = 6.1 - 4.4 \times 10^{-6} \times 125000 - 3.125 \times \left(\frac{125}{969} - 0.04 \right) - \left(0.021 - 1.8 \times 10^{-8} \times 125000 \right) \times 80$$

$$= 3.772$$

$$L = 10^{3.772} = 5916 \text{ hours}$$

07 > Fitting of Bearings

The Importance of Fitting

The function of a bearing can only be utilized to the full when it is fitted appropriately to a shaft and a housing. If there is insufficient interference on the fitting surface, the ring will become misaligned in the circumferential direction to the shaft or the housing. This phenomenon is called "creep," which may cause significant wear to the fitting surface, and damage the shaft or the housing. In some cases, this may even allow worn-off debris to enter the raceway, which may result in vibration and abnormal heating. In general, creep is generated on the ring where interference fit is used.

In order to prevent creep from taking place, necessary interference should be provided to the ring that receives the rotating load. Normally, interference is not provided to a ring that receives a static load. However, it is recommended to use an interference fit for both the inner and outer rings when using the bearing for applications subject to severe vibration.

Rotating ring	Load	Load conditions	Fitting
	Static	Inner ring rotating load Outer ring static load	Inner ring interference fit Outer ring clearance fit
	Rotating		
	Static	Outer ring rotating load Inner ring static load	Inner ring clearance fit Outer ring interference fit
	Rotating		
When load direction changes or there is an unbalanced load	Rotating or static	Indeterminate direction load	Inner and outer rings interference fit

Fitting between bearing and shaft

Conditions (steel solid shaft)	Shaft diameter range	Shaft tolerance class		
		Thin-section	Other	
Inner ring rotating load or indeterminate direction load	Light load of 0.06 C _r or less and fluctuating load	d ≤ 18	h5	js5
		18 ≤ d ≤ 30	h5	js5
		30 ≤ d ≤ 50	h5	js5
	Normal load of 0.06 to 0.12 C _r	d ≤ 18	js5	j5
		18 ≤ d ≤ 30	js5	k5
		30 ≤ d ≤ 50	js5	k5
Outer ring rotating load	The inner ring must be able to travel over the shaft easily	Applicable to all shaft diameters	g5	g6
	The inner ring does not have to travel over the shaft easily	Applicable to all shaft diameters	h5	h6

Fitting between bearing and housing

Conditions (integrated housing)	Travel of outer ring in axial direction	Housing tolerance class	
		Thin-section	Other
Inner ring rotating load	Various loads	H6	H7
	Light or normal load	H7	H8
	Temperatures of inner ring and shaft increase	G6	G7
	Precise rotation in light or normal load required	Cannot travel in principle	K5
Can travel		JS6	J6
Indeterminate direction load	Quiet operation required	H6	H6
	Light or normal load	JS6	J7
	Normal or heavy load	K5	K7
	Large impact load	M5	M7
Outer ring rotating load	Light or fluctuating load	M5	M7
	Normal or heavy load	N5	N7
	Thin-section housing and heavy load or large impact load	P6	P7

Fitting between miniature/small ball bearing (d < 10 mm) and shaft

Unit: μm

Load conditions	Bearing tolerance class	Single plane mean bore diameter deviation (Δ _{amp})		Dimensional tolerance of bearing diameter		Fitting		
		Maximum	Minimum	Maximum	Minimum	Interference	Clearance	
Inner ring rotating load	Mid to high speed Light to normal load	A5P, A7P, P5	0	-5	+2.5	-2.5	7.5	2.5
		P4	0	-4	+2.5	-2.5	6.5	2.5
	Low speed Light load	A5P, A7P, P5	0	-5	-2.5	-7.5	2.5	7.5
		P4	0	-4	-2.5	-7.5	1.5	7.5
Outer ring rotating load	Low to high speed	A5P, A7P, P5	0	-5	-2.5	-7.5	2.5	7.5
	Light load	P4	0	-4	-2.5	-7.5	1.5	7.5

Fitting between miniature/small ball bearing (d < 10 mm) and housing

Unit: μm

Load conditions		Bearing tolerance class	Single plane mean outside diameter deviation (Δ_{Dmp})		Dimensional tolerance of housing bore diameter		Fitting	
			Maximum	Minimum	Maximum	Minimum	Interference	Clearance
Inner ring rotating load	Mid to high speed Light to normal load	A5P, A7P, P5(※1), P4(※2)	0	-5	+5	0	0	10
		P5(18<D≤30)	0	-6	+5	0	0	11
		P4(18≤D)	0	-4	+5	0	0	9
	Low speed Light load	A5P, A7P, P5(※1), P4(※2)	0	-5	+2.5	-2.5	2.5	7.5
		P5(18<D≤30)	0	-6	+2.5	-2.5	2.5	8.5
		P4(18≤D)	0	-4	+2.5	-2.5	2.5	6.5
Outer ring rotating load	Low to high speed Light load	A5P, A7P, P5(※1), P4(※2)	0	-5	+2.5	-2.5	2.5	7.5
		P5(18<D≤30)	0	-6	+2.5	-2.5	2.5	8.5
		P4(18≤D)	0	-4	+2.5	-2.5	2.5	6.5

Note:

(1) applies to Class P5 (size: 18 ≤ D).

(2) applies to Class P4 (size: 18 < D ≤ 30).

Shaft dimensional tolerance

※ Single plane mean bore diameter deviation of bearing (P0 class)

Unit: μm

Diameter classification		Δ_{Dmp} (※)	Shaft Tolerances																							
More than	Or less		d6	e6	f6	g5	h5	h6	h7	h8	h9	h10	js5	js6	j5	j6	j7	k5	k6	k7	m5	m6	n6	p6	r6	r7
3	6	0 -8	-30 -38	-20 -28	-10 -18	-4 -9	0 -5	0 -8	0 -12	0 -18	0 -30	0 -48	±2.5	±4	+3 -2	+6 -2	+8 -4	+6 +1	+9 +1	+13 +1	+9 +4	+12 +4	+16 +8	+20 +12	+23 +15	+27 +15
6	10	0 -8	-40 -49	-25 -34	-13 -22	-5 -11	0 -6	0 -9	0 -15	0 -22	0 -36	0 -58	±3	±4.5	+4 -2	+7 -2	+10 -5	+7 +1	+10 +1	+16 +6	+12 +6	+15 +10	+19 +15	+24 +15	+28 +19	+34 +19
10	18	0 -8	-50 -61	-32 -43	-16 -27	-6 -14	0 -8	0 -11	0 -18	0 -27	0 -43	0 -70	±4	±5.5	+5 -3	+8 -3	+12 -6	+9 +1	+12 +1	+19 +7	+15 +7	+18 +12	+23 +18	+29 +23	+34 +23	+41 +23
18	30	0 -10	-65 -78	-40 -53	-20 -33	-7 -16	0 -9	0 -13	0 -21	0 -33	0 -52	0 -84	±4.5	±6.5	+5 -4	+9 -4	+13 -8	+11 +2	+15 +2	+23 +2	+17 +8	+21 +8	+28 +15	+35 +22	+41 +28	+49 +28
30	50	0 -12	-80 -96	-50 -66	-25 -41	-9 -20	0 -11	0 -16	0 -25	0 -39	0 -62	0 -100	±5.5	±8	+6 -5	+11 -5	+15 -10	+13 +2	+18 +2	+27 +2	+20 +9	+25 +9	+33 +17	+42 +26	+50 +34	+59 +34

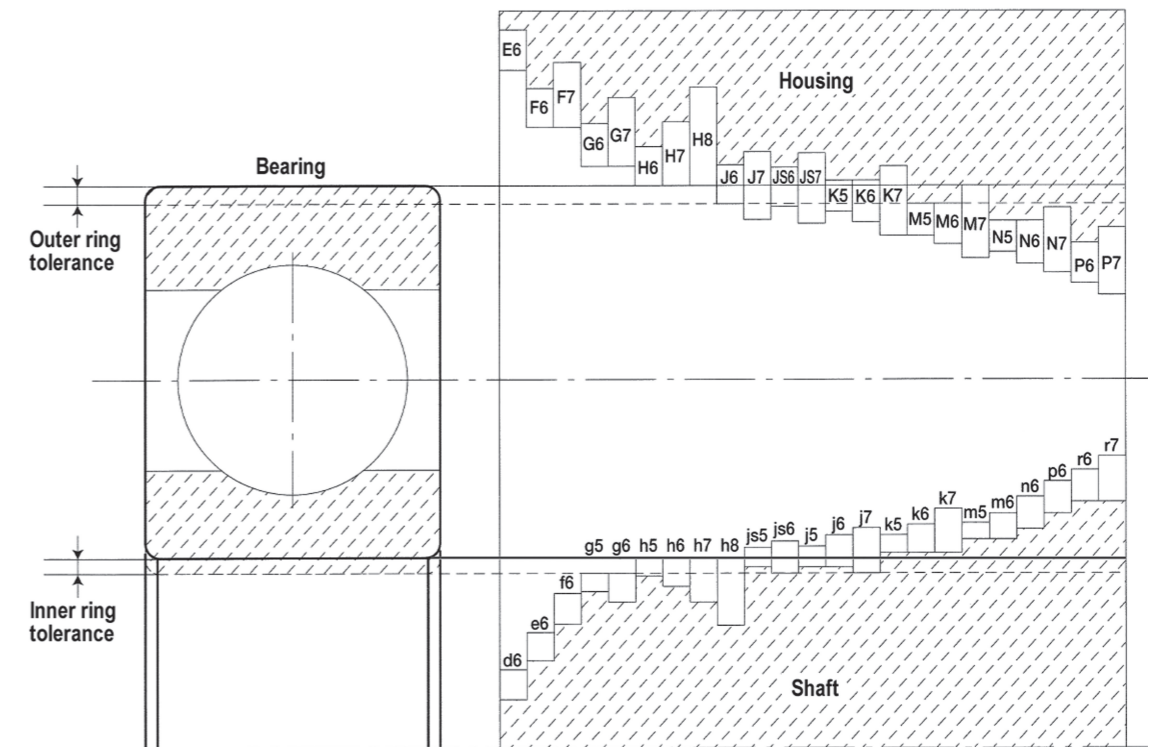
Housing bore dimensional tolerance

※ Single plane mean outside diameter deviation of bearing (P0 class)

Unit: μm

Diameter classification		Δ_{Dmp} (※)	Housing Tolerances																											
More than	Or less		E6	F6	F7	G6	G7	H6	H7	H8	J6	J7	JS6	JS7	K5	K6	K7	M5	M6	M7	N5	N6	N7	P6	P7					
10	18	0 -8	+43 +32	+27 +16	+34 +16	+17 +6	+24 +6	+11 0	+18 0	+27 0	+6 -5	+10 -8	±5.5	±9	+2 -6	+2 -9	+6 -12	-4 -12	-4 -15	0 -18	-9 -17	-9 -20	-5 -23	-15 -26	-11 -29					
18	30	0 -9	+53 +40	+33 +20	+41 +20	+20 +7	+28 +7	+13 0	+21 0	+33 0	+8 -5	+12 -9	±6.5	±10.5	+1 -8	+2 -11	+6 -15	-5 -14	-4 -17	0 -21	-12 -21	-11 -24	-7 -28	-18 -31	-14 -35					
30	50	0 -11	+66 +50	+41 +25	+50 +25	+25 +9	+34 +9	+16 0	+25 0	+39 0	+10 -6	+14 -11	±8	±12.5	+2 -9	+3 -13	+7 -18	-5 -16	-4 -20	0 -25	-13 -24	-12 -28	-8 -33	-21 -37	-17 -42					
50	80	0 -13	+79 +60	+49 +30	+60 +30	+29 +10	+40 +10	+19 0	+30 0	+46 0	+13 -6	+18 -12	±9.5	±15	+3 -10	+4 -15	+9 -21	-6 -19	-5 -24	0 -30	-15 -28	-14 -33	-9 -39	-26 -45	-21 -51					

Correlation diagram of shaft/housing and bearing



Calculating the Fit

The optimum fit should be selected for each application after considering a number of conditions such as the load size, rotation conditions, temperature conditions, and how the bearing is mounted/dismounted. Be sure to allow a greater interference than normal when a bearing is mounted on a thin housing, soft material, or a hollow shaft.

(1) Load size and interference

The interference between the shaft and the inner ring decreases when a radial load is applied. The amount of decrease can be obtained by the following equations, and the larger value should be adopted.

$$\Delta d_f = 0.08 \times (d/B \times F_r)^{0.5} / 1000 \text{ (mm)}$$

$$\Delta d_f = 0.02 \times F_r / B / 1000 \text{ (mm)}$$

(2) Impact of temperature of bearing and shaft/housing

The operation of the bearing generates temperature differences among the bearing's inner ring, outer ring, and balls, which cause a change in the interference with the shaft/housing. When the temperature difference between the bearing's interior and around the housing is ΔT , the temperature difference between the shaft and the bearing's fitting surface is assumed to be $(0.1 \sim 0.15) \times \Delta T$. Therefore, the amount of decrease of the inner ring's interference at this temperature (Δd_T) can be obtained by the following equation:

$$\Delta d_T = (0.1 \sim 0.15) \times \Delta T \times a \times d \doteq 0.0015 \times \Delta T \times d / 1000 \text{ (mm)}$$

Conversely, the interference between the outer ring and the housing may increase due to differences in temperature and the rate of expansion. When using a housing material with a large coefficient of linear expansion, such as aluminum or zinc, typically the interference increases at a low temperature.

(3) Effective interference and finish of fitting surface

The roughness of a fitting surface is compressed due to fitting, resulting in smaller degree of effective interference than nominal. The amount of decrease from the nominal interference varies depending on how the fitting surface is finished. In general, however, the effective interference can be obtained by the following equations:

$$\text{[Ground shaft]} \dots \Delta d = d / (d+2) \times \Delta d_a \text{ (mm)}$$

$$\text{[Turned shaft]} \dots \Delta d = d / (d+3) \times \Delta d_a \text{ (mm)}$$

After merging the above equations, the nominal interference required for the inner ring and the shaft with inner ring rotating load can be obtained by the following equation:

$$\Delta d_a \geq (\Delta d_f + \Delta d_T) \times ((d+3)/d \text{ or } (d+2)/d) \text{ (mm)}$$

(4) Surface pressure and maximum stress of fitting surface

If a bearing is mounted with interference, the ring will not break and remain secure provided the circumferential direction stress of the fitting surface is 120 MPa (12 kgf/mm²) or less.

Surface pressure P_m (MPa)	
Shaft and inner ring	(Hollow shaft) $P_m = (E \times \Delta d_b \times (1 - (d/d_b)^2) \times (1 - (d/d)^2)) / (2 \times d \times (1 - (d/d_b)^2))$ (Solid shaft) $P_m = E \times \Delta d_b / (2 \times d) \times (1 - (d/d_b)^2)$
Housing and outer ring	($D_h \neq \infty$) $P_m = (E \times \Delta D_a \times (1 - (D/D)^2) \times (1 - (D/D_h)^2)) / (2 \times D \times (1 - (D/D_h)^2))$ ($D_h = \infty$) $P_m = E \times \Delta D_a / (2 \times D) \times (1 - (D/D)^2)$
Circumferential direction stress δ_i (MPa)	
Shaft and inner ring	(Hollow shaft) $\delta_i = (E \times \Delta d_b \times (1 + (d/d_b)^2) \times (1 - (d/d)^2)) / (2 \times d \times (1 - (d/d_b)^2))$ (Solid shaft) $\delta_i = E \times \Delta d_b / (2 \times d) \times (1 + (d/d_b)^2)$
Housing and outer ring	($D_h \neq \infty$) $\delta_i = E \times \Delta D_a \times (1 - (D/D_h)^2) / (D \times (1 - (D/D_h)^2))$ ($D_h = \infty$) $\delta_i = E \times \Delta D_a / D$

(5) Press-in force and pull-out force

The press-in force and pull-out force can be obtained by the following equation based on surface area, surface pressure and the coefficient of friction of the fitting surface.

$$K_p = \pi \times \mu \times P_m \times B \times (d \text{ or } D) \text{ (N)}$$

When the inner ring is pressed into the shaft, or when the outer ring is pressed into the housing... $\mu = 0.12$
 When the inner ring is pulled out from the shaft, or when the outer ring is pulled out from the housing... $\mu = 0.18$

● Meaning of symbols

- Δd_f = Amount of decreased interference due to load (mm)
- d = Nominal bearing bore diameter (mm)
- B = Nominal bearing width (mm)
- F_r = Radial load (N)
- Δd_T = Amount of decreased interference due to temperature difference (mm)
- ΔT = Temperature difference between bearing's interior and around the housing (°C)
- a = Coefficient of linear expansion (1/°C)
- Δd = Effective interference (mm)
- Δd_a = Nominal interference (mm)
- E = Steel's modulus of longitudinal elasticity = 208000 (MPa)
- C_{or} = Basic static load rating (N)
- Δd_b = Inner ring's effective interference (mm)
- d_o = Hollow shaft's bore diameter (mm); in the case of solid shaft $d_o = 0$ (mm)
- D_a = Outer ring's raceway diameter (mm); generally $D_a = (4 \times D + d) / 5$ (mm)
- D = Nominal bearing outer diameter (mm)
- D_h = Housing outer diameter (mm); for rigid body $D_h = \infty$
- K_p = Press-in force or pull-out force (N)
- μ = Fitting surface's coefficient of friction
- d_b = Inner ring's raceway diameter (mm); generally $d_b = (D + 4 \times d) / 5$ (mm)

Figure 1 shows the minimum interference required to prevent the occurrence of creep for the radial load ratio (F_r/C_{or}), when a turned shaft is pressed into the extra-thin-section 67 series at $\Delta T=30^\circ\text{C}$.

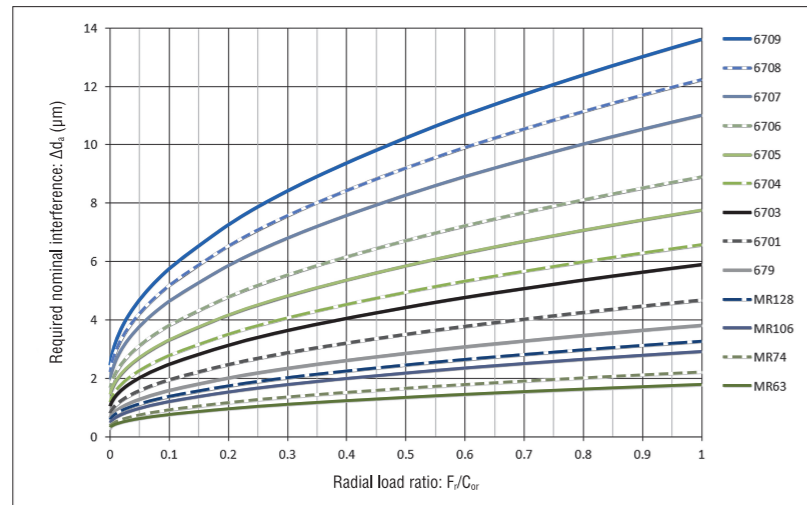


Figure 1: Radial load ratio and required nominal interference

Figure 2 shows the relation between the effective interference and the circumferential direction stress of the fitting surface, when the 67 series' inner ring is fitted with a solid shaft. The bearing will not break and will remain secure as long as the stress is $\sigma_t < 120$ (MPa). The points where each line graph intersects with the 120-MPa dashed line indicate the upper limit of effective interference.

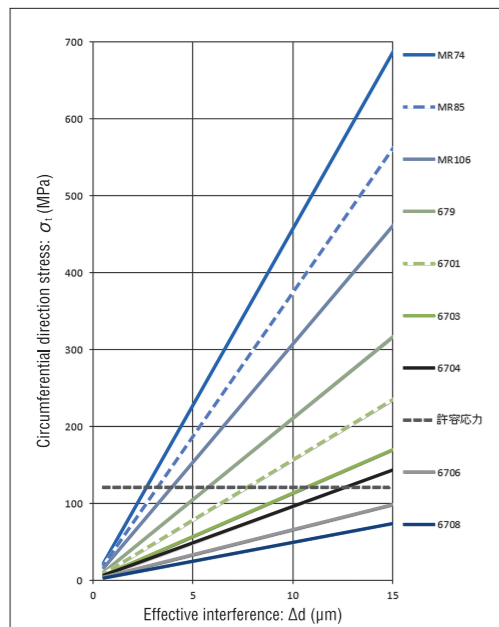


Figure 2: Effective interference and circumferential direction stress

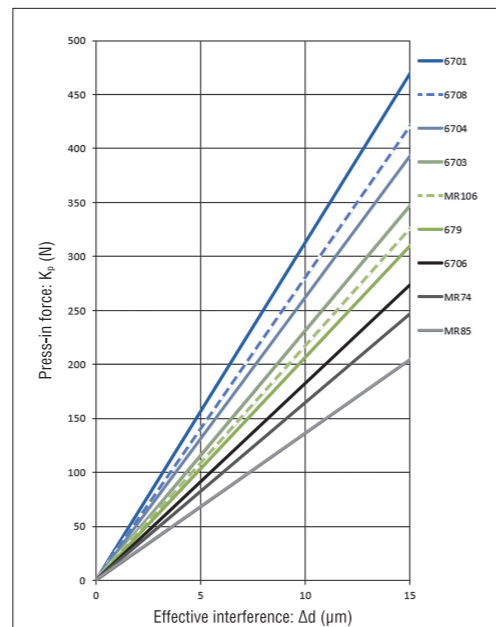


Figure 3: Effective interference and press-in force
 ※ Pull-out force is determined by multiplying press-in force by 1.5

Figure 3 shows the press-in force required under the same fitting conditions. The pull-out force can be determined by multiplying the press-in force by 1.5.

Precision and Roughness of Shaft and Housing

Normally, the shaft and the housing to be fitted to a bearing must satisfy the precision and surface roughness conditions below.

Recommended precision of shaft and housing

Classification	Symbol	Shaft	Housing
Circularity		Half or less of the shaft diameter tolerance	Half or less of the housing bore diameter tolerance
Cylindricity		Half or less of the shaft diameter tolerance within the range of bearing width	Half or less of the housing bore diameter tolerance within the range of bearing width
Perpendicularity		3/10000 (0.017°) or less	
Roughness of fitting surface	Ra	0.8	1.6

Type and symbol of geometric tolerance

Type	Symbol	
Shape	Straightness	
	Flatness	
	Circularity	
	Cylindricity	
	Line profile	
	Surface profile	
Direction	Parallelism	
	Perpendicularity	
	Inclination	
Position	Positionality	
	Coaxiality	
	Symmetry	
Swing		

Correspondence table of surface roughness values

Arithmetic mean roughness (Ra)	Maximum section height (Rt)	Roughness no.	Triangle symbol
0.025	0.15	N1	
0.05	0.3	N2	
0.1	0.6	N3	
0.2	1.2	N4	
0.4	2.4	N5	
0.8	4.8	N6	
1.6	9.6	N7	
3.2	19	N8	
6.3	38	N9	
12.5	75	N10	
25	150	N11	
(50)	(300)	N12	
(100)	(600)	N13	

Sort Categories of Bore/Outer Diameter Dimensions

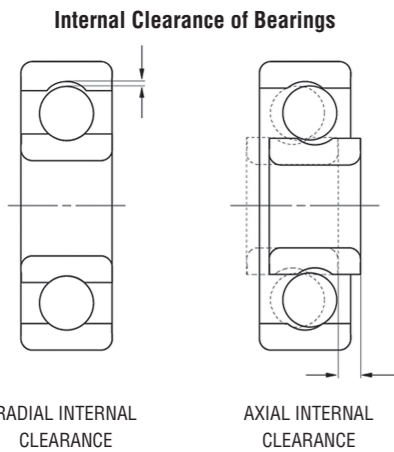
For applications where an excess of or shortage of interference may become a problem, upon your request, we can deliver the products sorted into two categories each for bore and outer diameter dimensions, as shown below.

TOLERANCES OF BORE DIAMETER (μm)	TOLERANCES OF OUTER DIAMETER (μm)	0 ~ -D/2	-D/2 ~ -D	0 ~ -D
	MARK		1	2
0 ~ -d/2	1	C11	C12	C10
-d/2 ~ -d	2	C21	C22	C20
0 ~ -d	0	C01	C02	

Remarks:
 1. Applied to P5, P4, ABEC5P, and ABEC7P bearings
 2. D=Lower limit of outer diameter dimensional tolerance
 3. d=Lower limit of bore diameter dimensional tolerance
 4. Let us know your requested details by selecting one option from below:
 ZC1...Sort only bore diameter into two categories
 ZC2...Sort only outer diameter into two categories
 ZC3...Sort both bore and outer diameters into two categories

08 > Internal Clearance of Bearings

Internal Clearance and Standard Values



Internal clearance is the space among a bearing's outer ring, inner ring, and balls. Generally speaking, the amount of vertical movement of the outer ring with the inner ring fixed is called the "radial internal clearance," and the amount of horizontal movement is called the "axial internal clearance." The amount of internal clearance during the bearing's operation is an important factor that impacts performance such as noise, vibration, heat generation, and fatigue life.

Deep groove ball bearings are usually classified by their radial internal clearance. In the actual clearance measurement, a designated load is applied to achieve stable results. As elastic deformation of the bearing occurs during the measurement, which makes the results larger than the true clearance, a correction (reduction) is made to obtain the true clearance.

Radial internal clearance of small/miniature bearings

Clearance symbol		MC1	MC2	MC3	MC4	MC5	MC6
Clearance	Minimum	0	3	5	8	13	20
	Maximum	5	8	10	13	20	28

Remarks:
 1. Standard clearance is MC3.
 2. The correction in the following table should be made when using the values above as measurement clearance.

Clearance symbol		MC1	MC2	MC3	MC4	MC5	MC6
Correction		1	1	1	1	2	2

Remarks: The measurement load is:
 1. For miniature bearings ... 2.5N (0.25kgf)
 2. For small bearings ... 4.4N (0.45kgf)

Radial internal clearance of standard deep groove ball bearings

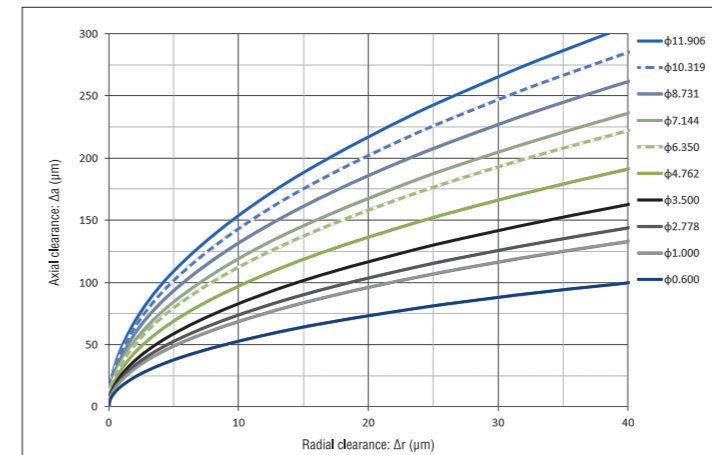
Nominal bearing bore diameter d (mm)		Radial internal clearance				
More than	Or less	C2	C0	C3	C4	C5
2.5	6	0~7	2~13	8~23	14~29	20~37
6	10	0~7	2~13	8~23	14~29	20~37
10	18	0~9	3~18	11~25	18~33	25~45
18	24	0~10	5~20	13~28	20~36	28~48
24	30	1~11	5~20	13~28	23~41	30~53
30	40	1~11	6~20	15~33	28~46	40~64
40	50	1~11	6~23	18~36	30~51	45~73
50	65	1~15	8~28	23~43	38~61	55~90
65	80	1~15	10~30	25~51	46~71	65~105
80	100	1~18	12~36	30~58	53~84	75~120

Nominal bearing bore diameter d (mm)		Measurement load N (kgf)	Clearance correction (μm)					
More than	Or less		C2		C0	C3	C4	C5
			Min.	Max.	Common	Common	Common	Common
2.5	18	24.5 (2.6)	3	4	4	4	4	4
18	50	49 (5)	4	5	6	6	6	6
50	80	147 (15)	6	8	8	9	9	9

Remarks:
 1. Standard clearance is C0.
 2. Corrections in the table above should be made when using the values above as measurement clearances.
 3. For the correction of C2 clearance, be sure to apply the minimum values to minimum clearance, and the maximum values to maximum clearance.

Relation between Radial Internal Clearance and Axial Internal Clearance

The axial internal clearance is determined based on the values of ball diameter, inner/outer ring raceway radius, and radial internal clearance. It is risky to select a bearing with a small radial internal clearance or a fitting with a large interference with the aim of achieving a smaller axial internal clearance after mounting.



Correlation between radial clearance and axial clearance according to ball diameter

$$\Delta_a \doteq 2 \times (\Delta_r \times (r_o + r_i - D_w))^{0.5}$$

Δ_a = Axial internal clearance (mm)
 Δ_r = Radial internal clearance (mm)
 D_w = Ball diameter (mm)
 r_o = Outer ring raceway radius (mm)
 r_i = Inner ring raceway radius (mm)

Selection of Bearing Clearance

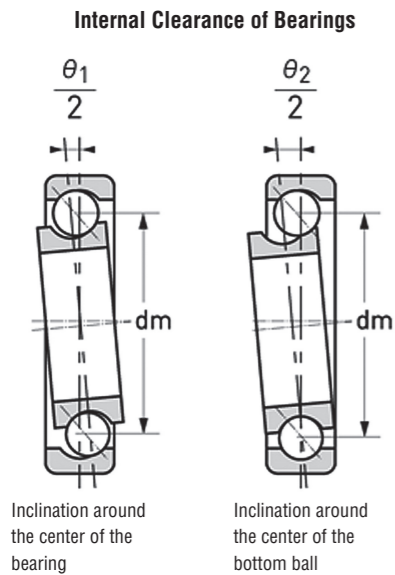
Theoretically, the longest bearing life can be achieved by setting the clearance during operation to a slightly negative value. However, it is also known that the life becomes significantly shorter when the negative clearance exceeds this value, even to the slightest degree. Therefore, normal practice is to select an initial clearance so that it becomes slightly positive (away from zero). Generally, MC3 is selected for miniature/small bearings, and C0 is selected for standard bearings.

Selection criteria for radial internal clearance

Conditions of use	Selected clearance
Clearance fit is used for both inner and outer rings; small axial load; rigidity in the axial direction is not required; clearance should be reduced without applying preload; vibration and noise should be reduced; and low-speed rotation.	MC1, MC2, C2
Friction torque should be decreased; normal axial load; normal rigidity in the axial direction; slight interference fit is used for the inner ring, and clearance fit is used for the outer ring; and mid- and low-speed rotation.	MC3, MC4, C0
Friction torque should be made particularly small; large axial load; rigidity in the axial direction is required; heavy load or impact load that requires interference; the inner ring's temperature is high, or the outer ring's temperature is low; and large shaft deflection.	MC5, MC6, C3, C4, C5

Relation between Radial Internal Clearance and Angular Clearance

During the actual use of a bearing, it may receive a moment load as a result of factors such as shaft deflection due to load and the housing's cylindricity. At this time, an inclination called the "angular clearance" is generated at the inner and outer rings. If the allowable angular clearance determined for each bearing is exceeded, this may cause an abnormal stress between the raceway and the ball, which will result in high temperatures or flaking.



Angular clearance refers to an angle that may be freely inclined when either the inner or outer ring is fixed, and when the ring that is not fixed is tilted to the left or right. The inclination around the center of the bearing is defined as θ_1 , and the inclination around the center of the bottom ball is defined as θ_2 . θ_1 is significantly larger than θ_2 . The angular clearance must be taken into account when designing the device and installing the bearing.

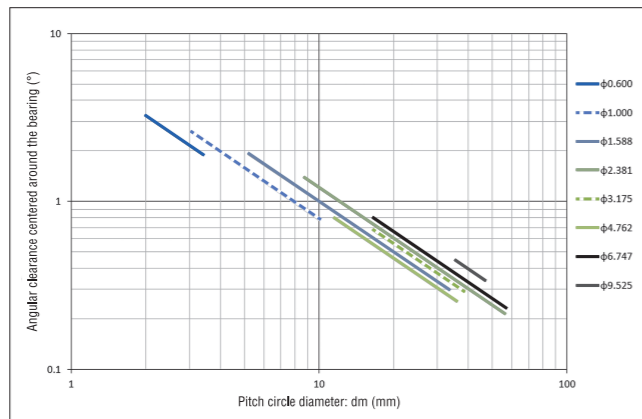
$$\theta_1 = 2 \times \tan^{-1} (2 \times (\Delta_r \times (r_o + r_i - D_w))^{0.5} / dm)$$

$$\theta_2 = 2 \times \tan^{-1} ((\Delta_r \times (r_o + r_i - D_w))^{0.5} / dm)$$

θ_1 = Angular clearance around the center of the bearing

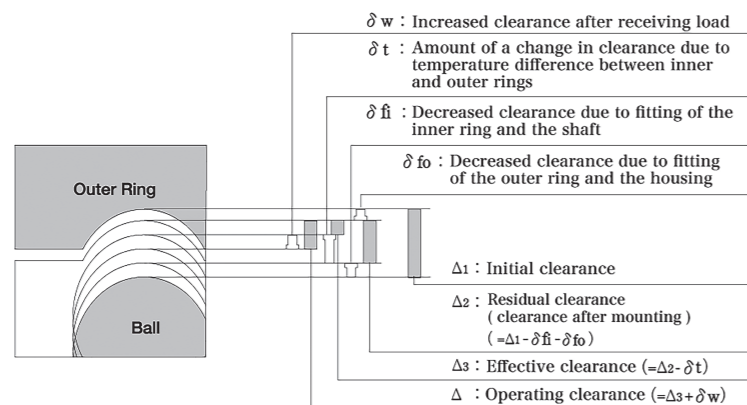
θ_2 = Angular clearance around the center of the bottom ball

dm = Pitch circle diameter (mm); generally $dm = (D+d)/2$



Pitch circle diameter and angular clearance according to ball diameter

Calculation of Clearance



(1) Operating clearance: Δ

Operating clearance refers to a clearance with elastic deformation caused by load and fitting during bearing operation at a constant temperature.

$$\Delta = \Delta_1 - (\delta_t + \delta_f) + \delta_w \text{ (mm)}$$

(2) Decreased clearance due to temperature difference between inner and outer rings: δ_t

Under normal operating conditions, the balls will have the highest temperature, followed by the inner ring, with the outer ring at the lowest temperature. It is difficult to measure the temperature of the balls, which is deemed to be identical to that of the inner ring for the sake of practical convenience.

$$\delta_t = a \times \Delta T \times D_a \text{ (mm)}$$

(3) Decreased clearance due to fitting: δ_f

When the bearing is mounted on a shaft or the housing with interference, the outer ring will contract, while the inner ring will expand, resulting in a decrease in the bearing's internal clearance.

$$\delta_f = \delta_{fi} + \delta_{fo} = \Delta d_b \times d / d_b \times ((1 - (d_o/d)^2) / (1 - (d_o/d_b)^2)) + \Delta D_a \times D_a / D \times ((1 - (D/D_h)^2) / (1 - (D_a/D_h)^2)) \text{ (mm)}$$

(4) Increased clearance after receiving load: δ_w

When a load is applied to the bearing, the internal clearance increases due to elastic deformation.

$$\delta_w = C \times ((0.51 \times F_r) / (Z \times \cos \alpha))^{(2/3)} \times (1/D_w)^{(2/3)} \text{ (mm)}$$

The contact angle α at this time can be obtained by the following equation:

$$\cos \alpha_o / \cos \alpha = 1 + C / (2 \times m - 1) \times (F_a / (9.8 \times Z \times D_w^2 \times \sin \alpha))^{(2/3)}$$

$$1 - \cos \alpha_o = \Delta_r / (2 \times D_w \times (2 \times m - 1))$$

● Meaning of symbols

ΔT = Temperature difference between inner and outer rings (°C); generally $\Delta T = 5$ to 10°C

D_a = Outer ring's raceway diameter (mm); generally $D_a = ((4 \times D + d)/5)$

Δd_b = Inner ring's effective interference (mm)

d_o = Hollow shaft's bore diameter (mm); in the case of solid shaft $d_o = 0$

ΔD_a = Outer ring's effective interference (mm)

d_b = Inner ring's raceway diameter (mm); generally $d_b = ((D + 4 \times d)/5)$

d = Nominal bearing bore diameter (mm)

D = Nominal bearing outer diameter (mm)

D_h = Housing outer diameter (mm)

Z = Number of balls

D_w = Ball diameter (mm)

α = Contact angle (°)

α_o = Initial contact angle (°)

Δ_r = Radial internal clearance (mm)

F_a = Axial load (N)

F_r = Radial load (N)

m = Average of inner/outer ring raceway groove curvature (mm)

a = Coefficient of linear expansion (1/°C);

when bearing steel is used: $a = 12.5 \times 10^{-6}$

when stainless steel is used: $a = 10.1 \times 10^{-6}$

C = Contact elastic modulus

Application category	C	m
Standard bearings	0.00218	0.525
Instrument bearings	0.00287	0.560

Axial Load and Axial Displacement, and Change in Contact Angle

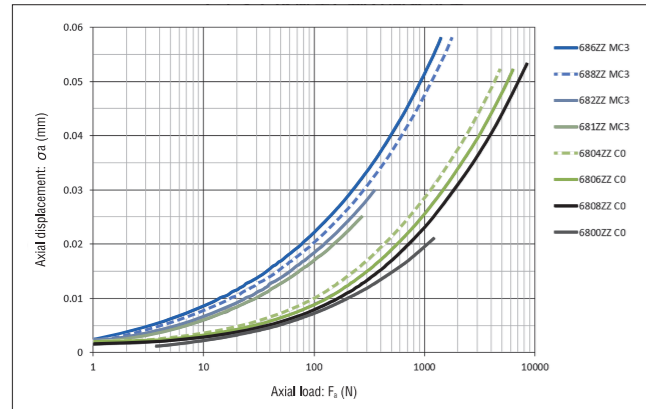
When the ball bearing receives an axial load, axial displacement takes place due to elastic deformation, and the contact angle becomes larger than the initial contact angle.

(1) Axial load: F_a

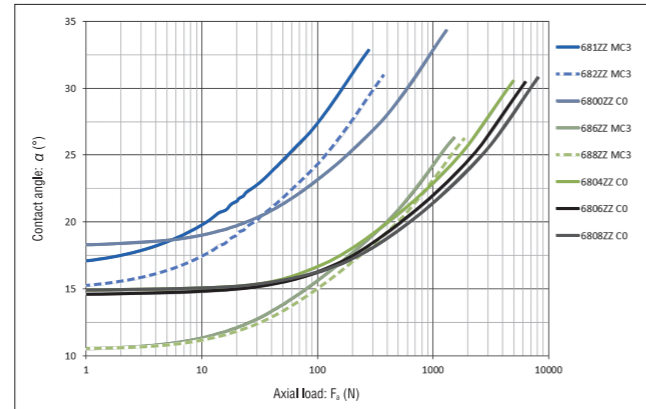
$$F_a = 9.8 \times Z \times \sin \alpha \times D_w^2 \times (\cos \alpha_0 / \cos \alpha - 1)^{(3/2)} \times ((2 \times m - D_w) / (C \times D_w))^{(3/2)} \text{ (N)}$$

(2) Axial displacement: δ_a

$$\delta_a = C / \sin \alpha \times (1 / D_w)^{(1/3)} \times (F_a / (Z \times \sin \alpha))^{(2/3)} \text{ (mm)}$$



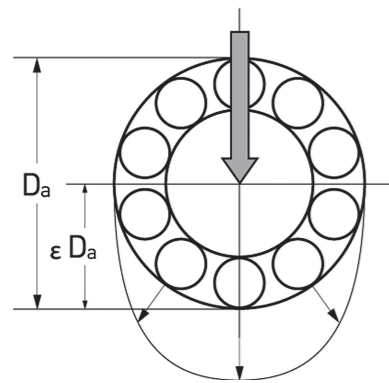
Axial load and axial displacement



Axial load and change in contact angle

Radial Clearance and Bearing Fatigue Life

Load distribution at $\epsilon=0.5$

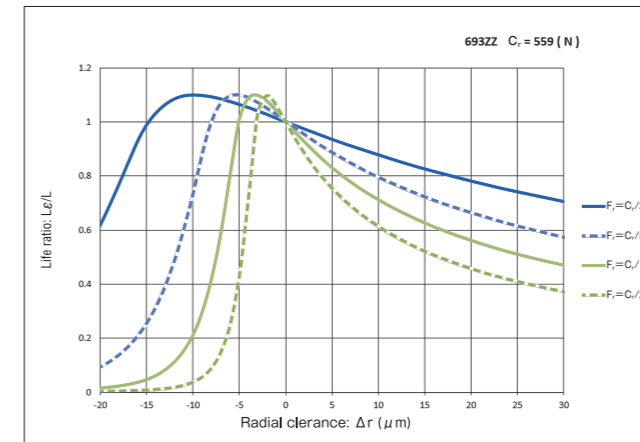


Normally, the radial clearance used for calculating the life of bearings is $\Delta_r = 0$, where the load distribution within the bearing can be represented by a load factor of $\epsilon = 0.5$. In this case, almost half of the balls receive the load. The load factor and the bearing fatigue life change based on the change of the radial clearance.

In the case of a deep groove ball bearing, the following relational equation is formulated between the radial clearance Δ_r and the load factor ϵ , and the function $F(\epsilon)$. L_ϵ can be obtained from the relation between $F(\epsilon)$ and the life ratio L_ϵ/L .

$$F(\epsilon) = \Delta_r \times D_w^{(1/3)} / (C \times (F_r/Z)^{(2/3)})$$

As shown in the example figure below, the longest life can be achieved when the clearance value is slightly negative. The figure also shows that as the clearance increases, the number of balls that receive the load decreases, which results in a shorter life.



Radial clearance and bearing fatigue life

L_ϵ = Bearing life when radial clearance is Δ_r
 L = Bearing life when radial clearance is $\Delta_r = 0$

ϵ	0.1	0.2	0.3	0.4	0.5	0.6	0.7	0.8	0.9	1
$F(\epsilon)$	33.7	10.2	4.05	1.41	0	-0.86	-1.44	-1.86	-2.2	-2.49
L_ϵ/L	0.29	0.55	0.74	0.89	1	1.07	1.1	1.09	1.04	0.95

ϵ	1.2	1.5	1.8	2	2.5	3	4	5	7	10
$F(\epsilon)$	-3.1	-3.88	-4.6	-5.05	-6.11	-7.09	-8.87	-10.5	-13.3	-17.2
L_ϵ/L	0.64	0.37	0.22	0.16	0.078	0.043	0.017	0.008	0.004	0.001

09 > Lubrication

Purpose of Lubrication

The life and performance of bearings change significantly depending on the selected lubrication methods and lubricants, so they must be chosen appropriately considering the conditions of use. Lubrication has the following effects:

(1) Decreased friction and wear

Lubrication decreases the rolling friction between the raceway surface and the balls, the sliding friction between the balls and the cage, and the sliding friction between the cage and the raceway guide surface.

(2) Removal of generated heat

Lubrication removes the frictional heat caused internally by rotation as well as other heat transmitted from outside, and prevents the heating of bearings and the deterioration of lubricants.

(3) Relaxation of stress and extension of fatigue life

Forming an appropriate lubricant film on the rolling contact surface during rotation relaxes the stress concentrated due to impact load, and extends the bearing's fatigue life.

(4) Rust-resistant and dust-resistant effect

Lubrication prevents the generation of rust on the balls, rings, and cage, and the intrusion of dust, foreign matter, and moisture into the bearing.

Requirements of a Lubricant

(1) Low friction and wear.

(2) High thermal stability and good thermal conductivity.

(3) High-strength lubricant film.

(4) Free of corrosive properties.

(5) Free of dust and moisture.

(6) Maintains viscosity suited to the conditions of use.

● Comparison between oil lubrication and grease lubrication

Item	Oil lubrication	Grease lubrication
Rotational speed	From low speed to high speed	Low speed and medium speed
Lubrication performance	Excellent	Good
Cooling effect	Good	None
Torque	Relatively small	Relatively large
Lubricant life	Long	Relatively short
Lubricant replacement	Easy	Difficult
Lubricant leakage	Not suited for places vulnerable to oil leaks	Small leakage contamination
Dust filtration	Easy	Difficult
Sealing device	Complicated	Simple

Standard Lubricants

The standard lubricants below are used unless specified otherwise:

Lubricant	Standard grease	Standard oil
Brand	Multemp SRL	AeroShell Fluid 12
Abbreviation	SRL	AF2
Manufacturer	Kyodo Yushi	Shell Lubricants Japan
Operating temperature range	-50 to 150°C	-54 to 135°C
Specific gravity	0.93	0.92

※Force-feed lubrication (oil bath, drip feeding, splash, circulation, and jet, etc.) should be performed as necessary when oil is used.

Grease

Grease is a semisolid lubricant that consists of base oil, thickener, and additive. Based on the combinations of these materials, you must select a grease that suits your application.

(1) Base oil

In general, the base oil of grease is mainly made from mineral oil. Synthetic oil, including silicone oil, diester oil, and fluorinated oil, is also used to improve the grease's heat resistance and low-temperature fluidity.

(2) Thickeners

Thickeners can be roughly classified into the soap type or the non-soap type, and have an impact on properties such as mechanical stability, water resistance, and operating temperature range.

(3) Additives

Various additives may be added depending on the purpose of use.

•An extreme pressure additive improves impact load and heavy load properties.

•An antioxidant prevents degradation due to oxidation caused when the grease is not resupplied for a long period of time.

•A corrosion inhibitor prevents the generation of rust on and around the bearings.

(4) Consistency

Consistency refers to the hardness of the grease, and it is measured by how deep a metal cone with a specified weight penetrates into the grease in five seconds, in 0.1-mm units. Larger numbers indicate that the grease is softer.

● Consistency and consistency number of grease

NLGI NO.	00	0	1	2	3	4
Worked penetration (25°C, 60 times)	400 – 430	355 – 385	310 – 340	265 – 295	220 – 250	175 – 205
Application	For intensive degreasing	For intensive degreasing	For intensive degreasing and low-temperature use	For general use	For general and high-temperature use	For high-temperature use
Condition	Semi-fluid	Very soft	Soft	Normal	Firm	Very firm

(5) Dropping point

Dropping point refers to the temperature at which the grease starts to drip from a hole with a specified size after the grease is heated to a fluid state. A higher dropping point indicates that the grease can be used at a higher maximum temperature environment.

(6) Mixing different types of grease

When different types of grease that contain different base oil, thickeners, and additives are mixed, their properties will change. Therefore, in principle, grease products from different brands should not be mixed.

● Types of grease that may or may not be mixed (reference)

Base oil	Ester oil	Mineral oil	Synthetic hydrocarbon oil	Silicone oil	Polyglycol oil	Fluorine oil
Ester oil	Yes	Yes	Yes	No	Yes	No
Mineral oil	Yes	Yes	Yes	No	No	No
Synthetic hydrocarbon oil	Yes	Yes	Yes	No	No	No
Silicone oil	No	No	No	Yes	No	No
Polyglycol oil	Yes	No	No	No	Yes	No
Fluorine oil	No	No	No	No	No	Yes

Thickener	Lithium soap	Calcium soap	Aluminium soap	Urea
Lithium soap	Yes	No	No	Yes
Calcium soap	No	Yes	No	Yes
Aluminium soap	No	No	Yes	No
Urea	Yes	Yes	No	Yes

(7) Amount of filled grease

We categorize the amount of filled grease according to the usage conditions as shown in the table below. The standard products are filled with grease G, L, or Q below, as defined in advance for each product model.

Grease amount symbol	Amount of filled grease (%)	Usage conditions	
		Speed	Load
F	90±10	Low	Heavy
M	70±10	Low	Heavy
S	50±10	Low	Normal
G	40±10	Medium	Normal
L	30±10	Medium	Normal
Q	25±5	Medium	Normal
K	20±5	High	Light
Y	15±5	High	Light
X	10±5	High	Light

(8) Grease life (reference)

The life of grease used in a sealed/shielded bearing can be obtained by the following equation:

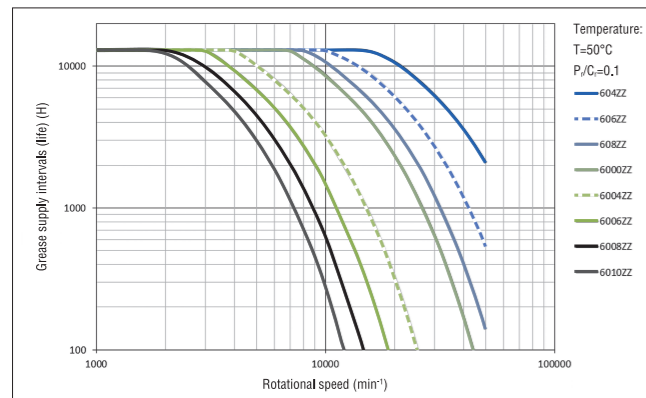
$$\log L = 6.1 - 4.4 \times 10^{-6} \times dm \times n - 3.125 (P_r/C_r - 0.04) - (0.021 - 1.8 \times 10^{-8} \times dm \times n) \times T$$

- (a) Applies when $T \leq 120^\circ\text{C}$
However, $T = 50^\circ\text{C}$ where $T < 50^\circ\text{C}$
- (b) Applies when $dm \times n \leq 5 \times 10^5$
However, $dm \times n = 1.25 \times 10^5$ where $dm \times n < 1.25 \times 10^5$
- (c) Applies when $P_r/C_r \leq 0.16$
However, $P_r/C_r = 0.04$ where $P_r/C_r < 0.04$

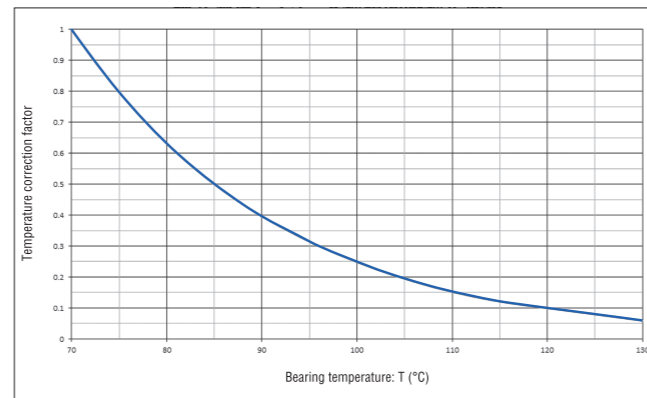
- L=Grease life (h)
- $dm = (D+d)/2$ (mm)
- n=Rotational speed (min^{-1})
- P_r =Dynamic equivalent radial load (N)
- C_r =Basic dynamic load rating (N)
- T=Bearing operating temperature ($^\circ\text{C}$)

(9) Grease relubrication intervals

Even when a high-quality grease is used, its properties will deteriorate and its lubrication performance will decrease depending on the usage conditions, such as the load, rotational speed, temperature, and ambient atmosphere, so you must supply or replace the grease in a timely manner. In general, it is desirable to replace the grease once a year at an operating temperature of 50°C , and two or three times a year at a temperature higher than 100°C , even when the grease is heat resistant. The figure below, titled Rotational speed and relubrication intervals (life), shows the relationship between the rotational speed and the relubrication intervals by bearing bore diameter. The figure below, titled Bearing temperature and correction factor for calculating relubrication intervals, indicates the relationship between the bearing temperature (above 70°C) and the correction factor, and this value should be multiplied by the relubrication interval.



Rotational speed and relubrication intervals (life)



Bearing temperature and correction factor for calculating relubrication intervals

● Properties of different types of grease

Properties			Appearance	Dropping point	Operating temperature range ($^\circ\text{C}$)	Water resistance	Mechanical stability	Remarks		
General name	Thickener	Base oil								
General-purpose grease	Li soap	Mineral oil	Butter-like	170 to 190	-30 to +120	Good	Good	Common general-purpose grease widely used for medium- and small-sized ball bearings.		
Diester grease		Diester oil	Fiber-like or butter-like		-50 to +130			Suited for low-temperature applications.		
Silicone grease		Silicone oil	Fiber-like or butter-like		220 to 260			-50 to +180	Wide operating temperature range from low to high, mainly used in light-load applications ($P_r/C_r \leq 3\%$).	
Cup grease	Ca soap	Mineral oil	Butter-like	80 to 100	-10 to +70	Good	Relatively good	Includes a small amount of water as structure stabilizer. Not suited for high-temperature applications.		
Fiber grease	Na soap	Mineral oil	Fiber-like or butter-like	160 to 180	0 to +110	Bad (emulsification)	Good	Emulsifies with water and becomes unusable. May be used in relatively-high-temperature applications.		
Mobile grease	Al soap	Mineral oil	Thread-like or butter-like	70 to 90	-10 to +80	Good	Relatively good	Highly adhesive and suited for use in locations subject to vibrations.		
Mixture grease	Ca+Na soap, etc.	Mineral oil	Butter-like	150 to 180	-10 to +120	Bad (when Na is used)	Good	Applied to large-sized bearings.		
Composite grease	Li composite soap, etc.	Mineral oil	Fiber-like or butter-like	180 to 300	-20 to +130	Good	Good	Suited for high-temperature and high-load applications.		
Non-soap grease	Benton	Mineral oil or synthetic oil	Butter-like	230 and higher	-10 to +150	Good	Good	Suited for high-temperature and high-load applications.		
	Silica gel							Relatively good	Relatively good to bad	Has low water resistance.
	Urea							Good	Good	Suited for high-temperature applications.

Lubricant Oil

Mineral oil and synthetic oil generally have high-strength lubricant film, high oxidation stability, and rust-resistant properties, so these oils are used to lubricate the bearings. A lubricant oil with an appropriate viscosity for the relevant usage conditions must be selected. The desirable kinematic viscosity at the bearing's operating temperature is $13\text{mm}^2/\text{s}$ or higher.

If the viscosity of the lubricant oil is too low, this will cause an oil film shortage, resulting in wear and/or seizure. On the other hand, if the viscosity is too high, this will increase the torque and generate heat. In general, high-viscosity oil should be used for high-load and high-operating-temperature applications, and low-viscosity oil should be used for high-speed applications.

As with grease, you should carefully consider when to replace the lubricant oil and whether to mix it with different brands.

● Lubricant oil selection criteria

Bearing operating temperature ($^\circ\text{C}$)	dn value	ISO viscosity grade (VG) of the lubricant oil	
		Normal load	Heavy load or impact load
-30~0	Up to the limiting speed	15, 22, 32	32, 46
0~60	Up to 15000	32, 46, 68	100
	15000~80000	32, 46	68
	80000~150000	22, 32	32
	150000~500000	10	22, 32
60~100	Up to 15000	150	220
	15000~80000	100	150
	80000~150000	68	100, 150
	150000~500000	32	68
100~150	Up to the limiting speed	320	

Remarks:

- In general, high-viscosity lubricant oil should be used for heavy-load and low-speed applications.
- The figures in this table apply to oil bath and circulation lubrication systems.
- The dn value is: bearing bore diameter d (mm) \times rotational speed n (min^{-1}).
- When using oil lubrication, an appropriate lubrication method for the application (such as oil bath, drip feeding, splash, circulation, oil mist, and jet, etc.) must be implemented.

10 > Limiting Speed of Bearings

Each bearing has its own rotational speed limit. The empirical speed limit up to which the bearing can continue to operate stably without causing any problems, even when the bearing's internal friction generates heat, is called the "limiting speed." The limiting speed varies according to the conditions such as the types of bearings and cages, lubrication method, bearing load, and cooling conditions around the bearing.

The limiting speed of bearings that use the contact rubber seals (2RS) is limited by the circumferential velocity at the seal contact part, so can be lower than that of the non-contact-type bearing.

When the bearing is operated under a large load, the limiting speed must be made smaller. When the bearing is not used under normal load conditions, the limiting speed must be multiplied by the correction factor shown in the table below ($C_i/P < 12$ and $F_a/F_r > 0.2$).

The limiting speed of duplex bearings is about 20% of the limiting speed of a single bearing. When a nylon cage is used, the limiting speed may be 1.5 times faster, compared to when a steel cage is used for the bearing.

● Correction of limiting speed according to the bearing's load

C_i/P	5	6	7	8	9	10	11	12
Correction factor	0.72	0.79	0.85	0.9	0.93	0.96	0.98	1

● Correction of limiting speed under combined load

F_a/F_r	0.25	0.5	0.75	1	1.25	1.5	1.75	2
Correction factor	1	0.95	0.93	0.91	0.89	0.88	0.87	0.86

In addition, the limiting speed must be multiplied by the correction factor in the table below to obtain the final limiting speed, depending on whether the bearing uses outer ring rotation or inner ring rotation, and whether the lubricant is grease or oil.

● Correction of limiting speed depending on the rotating ring and lubricant

Lubricant	Rotating ring	
	Outer ring	Inner ring
Grease	0.6	1
Oil	0.8	1

You may want to refer to the usage conditions below when the sealing device is embedded in the shaft or the housing (not in the bearing itself), and when nitrile rubber seal is used.

● Usage conditions of nitrile rubber seals

Shaft diameter (mm)	≤10	≤20	≤30	≤40
Shaft circumferential velocity (m/s)	≤8	≤10	≤12	≤14
Shaft surface roughness (Rt)	≤3.2	≤2.4	≤1.6	≤0.8
Shaft surface hardness (HRC)	For low speed ≥35, for high speed ≥50			
Operating temperature range (°C)	-40~+120			

11 > Friction Torque

Friction Torque (reference)

The friction torque of a rolling bearing changes according to the bearing load and lubrication conditions. Furthermore, when grease is used as the lubricant, grease resistance is added to the bearing's friction torque. If the bearing's load is normal ($C_i/P > 12$ and $F_a/F_r < 0.2$) and the bearing is well lubricated (oil lubrication), the bearing's friction torque during operation can be obtained by the following equation:

$$M = \mu \times P_r \times d / 2$$

M=Friction torque (N · mm)

μ =Coefficient of friction

P_r =Radial load (N)

d=Bearing bore diameter (mm)

Bearing Type	Coefficient of friction: μ
Deep groove ball bearing	0.0013
Angular contact ball bearing	0.0015
Thrust ball bearing	0.0011

Temperature Increase

When the bearing is used, its temperature increases due to rotational friction and the grease's agitation resistance. In general, the temperature increases rapidly at the beginning of operation, but the temperature eventually becomes steady due to factors such as the dissipation of heat from the shaft and the housing, and the cooling effect achieved by the lubrication. If the temperature increase continues for a long period of time, this will result in a shorter life owing to factors such as decreased bearing clearance, decreased rotational accuracy, and degraded lubricant.

Therefore, when such a state is detected, you must review and reconsider the selected bearing specifications, the setup and structure around the bearing, the lubricant and lubrication method, and other factors.

12 > Preload

Preload may be applied when a high dynamic rotational accuracy is required of the bearing, and when low vibration and noise, and a high impact resistance are required. Preload can be applied by inserting a spring, shim, or spacer, or by grinding the face of the outer or inner ring to achieve the desirable preload amount of the two bearings.

(1) Back-to-back duplex (DB)

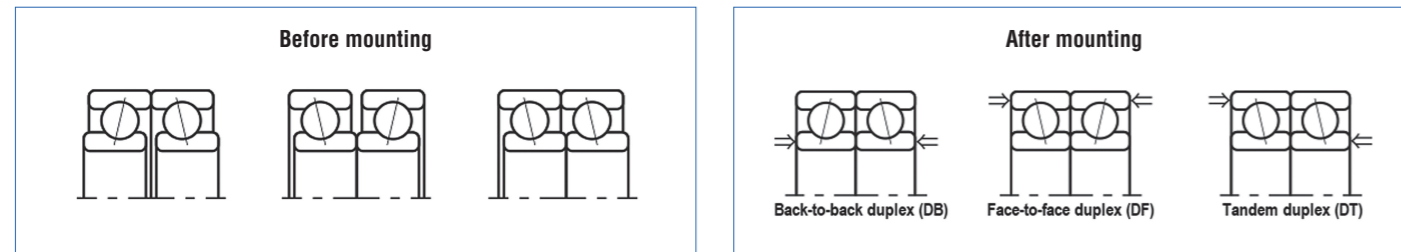
- As the line of action faces outward, a high moment load resistance is achieved.
- As the positioning in the radial and axial directions are accurate, the displacement may be controlled easily.

(2) Face-to-face duplex (DF)

- As the line of action faces inward, the moment load resistance becomes smaller than the DB duplex, but the shaft inclination can be absorbed easily.
- As the positioning in the radial and axial directions are accurate, the displacement may be controlled easily.

(3) Tandem duplex (DT)

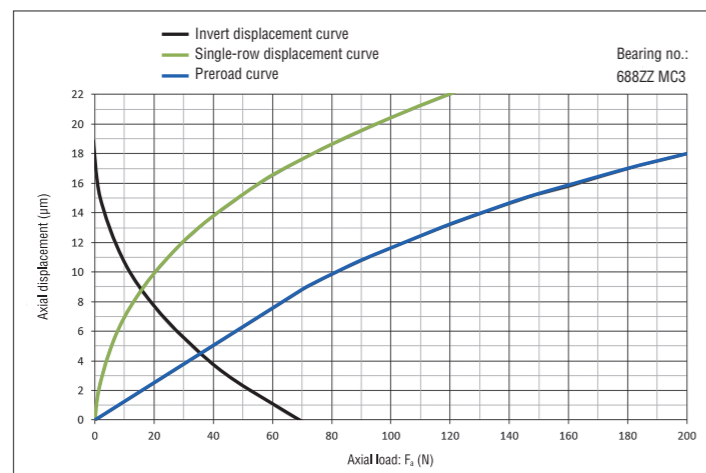
- This is used to increase the load capacity and rigidity. However, as the tandem duplex can receive radial load and unidirectional axial load only, the axial load in the opposite direction must be received by using another bearing.



● Standard preload amount

Preload category	Preload amount		Features
	Miniature and small bearing	Standard bearing	
Slight preload (S)	$0.50\% \times C_r$	$0.15\% \times C_r$	Bearing rigidity not required, emphasis on low torque
Light preload (L)	$1.25\% \times C_r$	$0.58\% \times C_r$	Bearing rigidity and low torque are both required
Medium preload (M)	$1.75\% \times C_r$	$1.28\% \times C_r$	Emphasis on bearing rigidity, relatively high torque
Heavy preload (H)	$2.50\% \times C_r$	$2.64\% \times C_r$	Emphasis on bearing rigidity, high torque

※ C_r = Basic dynamic load rating (N)



Axial load and axial displacement of duplex bearings

13 > Basic Rules for Selecting and Handling Bearings

Selection of Bearings

- (1) The performance of a thin-section bearing heavily relies on the accuracy of the shaft and housing. The accuracy around the bearing must fully meet the conditions indicated in the fittings chart. Particularly, if you have any questions regarding the use of 6700 and 6800 series products, feel free to consult with us.
- (2) If you are planning to use a bearing with a snap-type (W) cage for high-acceleration, heavy-load, and impact-load applications, for the vertical shaft, and/or with force-feed oil lubrication, and if you have any questions, feel free to consult with us.
- (3) You must select the fitting, clearance, lubrication method, and lubricant carefully by fully taking into account the rotational speed, load, and temperature, in order to prevent anomalies such as seizure, premature flaking, and large noise from taking place.
- (4) Full complement ball bearings are suited for low-speed and heavy-radial-load applications. You must fully comply with the usage conditions because the balls may fall out of the slot groove with a relatively small axial load.

Handling and Storage of Bearings

- (1) In order to prevent the formation of rust, bearings should be stored in an environment at a temperature of around 20°C and a humidity of 65% or less. Do not place them directly on the floor (it is desirable to store the bearings on a shelf at least 30 cm above floor), avoid direct sunlight and contact with cold wall surfaces.
- (2) The bearings should be handled in a clean environment, making sure any sweat or dirt from your hands do not get attached. Also, bearings should be handled by those with extensive knowledge on bearings, based on the defined work standard. Above all, the bearings must be handled carefully to avoid any damage, indentation, and chipping.
- (3) Placing the bearings in an acidic atmosphere may result in rust and discoloration. Also, if you use cotton work gloves or waste cloth to wipe the bearing, shaft, or housing, dust may enter the bearing or the fitting, which may cause anomalies. Make sure to avoid these situations.

Mounting

(1) Precautions before mounting

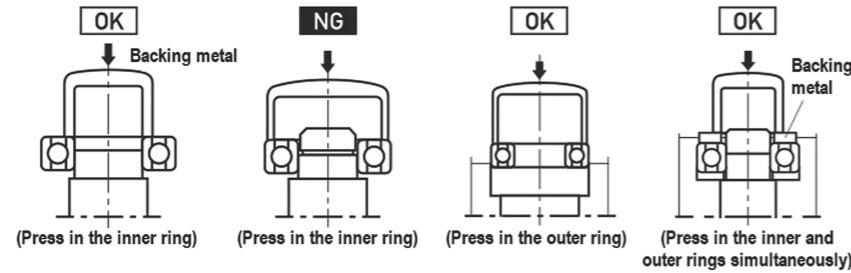
- a) The bearing should be mounted in a clean environment, using clean mounting jigs and tools.
- b) When mounting a new bearing, do not open its package until immediately before the mounting process.
- c) Make sure to seal the container of the oil or grease to be used.
- d) Wash the shaft and housing, and check in advance that they are free of any damage, indentation, and deformation.
- e) When using grease lubrication, use the bearing directly without washing it.
- f) When using an open bearing, wash off the corrosion inhibiting oil and apply an appropriate lubricant before use. Feel free to consult with us if you wish to have the product filled with a lubricant before shipping.

(2) Shaft and housing inspection

- a) Check whether the dimensions, accuracy, and finish surface roughness of the shaft and housing are in accordance with the designated specifications. If the fitting surface is too rough, the fitting may loosen during use, which may cause creep. If the roundness of the corners is larger than the bearing chamfer r_{min} , or the shoulder surface is inconsistent, the bearing cannot be mounted perpendicularly, which will cause a large moment load and deviated rotation, resulting in a shorter life.
- b) The shaft length changes depending on the temperature; therefore, when two or more bearings are mounted on a shaft for use, the normal practice is to fix one bearing and allow another bearing to move within the housing. If this is the case, you must check that the clearance in the axial direction allows this bearing to move.

14 > Problems in Bearings, and their Causes and Remedies

How to Mount a Bearing



(1) Inner ring interference fit

A press machine should be used to press in small bearings with inner ring rotating load and small interference. When a large interference and/or a large bearing are used, shrink fit should be performed at a temperature of 120°C or less either in oil or by using an induction-heating device, etc.

(2) Outer ring interference fit

A press machine should be used to press in small bearings with outer ring rotating load and small interference. When a large interference and/or a large bearing are used, cooling fit should be performed, using dry ice and the like. In this case, you must consider introducing waterproofing measures to prevent rusting.

(3) Outer and inner rings' interference fit

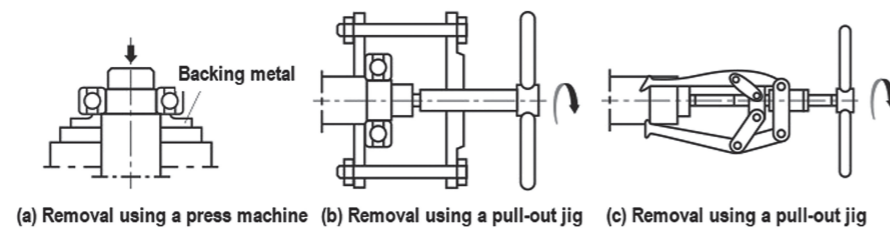
When the outer and inner rings must be pressed in at the same time, a backing metal should be used to enable simultaneous contact of the inner/outer rings' faces. Before the press-in process, you may want to apply high-precision oil onto the fitting surfaces of the shaft and housing.

Operation Check

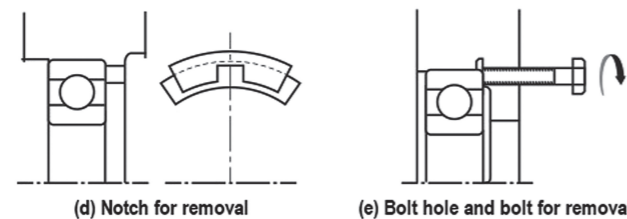
- Small devices should be rotated manually to check that they are free of any excessive torque, uneven rotation, and snags.
- Devices that cannot be rotated manually should be started with no load and immediately switched to coasting, then you should perform the checks as with (1) above.
- If no anomalies are found in (1) or (2) above, conduct a powered trial run where the power is increased slowly from no load and low speed to standard rotation. Here, you should check that there are no anomalies in terms of temperature rise and vibrations.

How to Remove a Bearing

(1) In case you may need to remove the interference fit bearing in the future with an aim to reuse it or investigate the cause of a defect, you should design and create a dedicated jig so that you will be able to remove the bearing easily without causing any damage.



(2) When using a press machine to remove the inner ring of the interference fit, you should place a backing metal against the inner ring. In addition, if a shaft design that can be grappled is employed, you may be able to use a puller to remove the bearing.



(3) For removal of the outer ring of the interference fit, it is recommended to create a bolt screw hole or a notch at the shoulder of the housing.

Operational Abnormality	Cause	Remedy	
Noise	High-pitched metallic noise	Poor lubrication	Use the correct amount of appropriate lubricant
		Insufficient clearance	Ensure proper clearance
		Poor mounting	Check the accuracy of the shaft and housing, as well as the mounting method
		Excessive load	Check the fitting and preload
	Low-pitched metallic noise	Indentation on raceway surface	Avoid the impact load when dropped or during mounting
		Rust and/or damage	Check the sealing device, and use clean lubricant
	Regular noise	Flaking on raceway surface	Use appropriate fitting, clearance, lubrication and mounting method
		Irregular noise	Intrusion of foreign matter
	Excessive clearance		Ensure proper clearance
	Ball damage and ball flaking		Ensure proper clearance and load
	Noise that changes over time	Change in clearance due to rising temperature	Check the shaft and housing materials, and ensure proper clearance
		Ongoing abnormality on the raceway	Use appropriate fitting, clearance, lubrication and mounting method
Heavy vibration	Raceway and ball flaking	Use appropriate fitting, clearance, lubrication and mounting method	
	Intrusion of foreign matter	Check the sealing device, and use clean lubricant	
	Excessive clearance	Ensure proper clearance	
	Poor mounting	Adjust the perpendicularity of the shaft and housing shoulders	
Abnormal temperature rise	Insufficient clearance	Ensure proper clearance	
	Poor mounting	Check the accuracy of the shaft and housing, as well as the mounting method	
	Excessive load	Check the clearance, fitting, and preload	
	Poor lubrication	Use the correct amount of appropriate lubricant	
	Creep	Check the fitting, and adjust the shaft and housing	
Leakage and discoloration of lubricant	Too much grease	Use the correct amount of appropriate lubricant	
	Intrusion of foreign matter	Check the sealing device, wash the parts around the bearing, and replace the bearing	

Technical Contents 13 Basic Rules for Selecting and Handling Bearings 14 Problems in Bearings, and their Causes and Remedies

15 > Damage to Bearings, and its Causes and Remedies

Inappropriate handling or use of bearings often results in damage and a shortened life. This section highlights the common causes of trouble and preventative remedies.

Damage	Damage Symptoms	Cause	Remedy
Flaking	Flaking over the entire circumference on one side of the raceway	Abnormal axial load	Use clearance fit for the outer ring of the non-fixed bearing
	Ball-pitch flaking on the raceway	Impact load during mounting	Carefully mount the bearing
		Rust generated during downtime	Apply rust-proof treatment when a long downtime is scheduled
	Premature flaking on the raceway surface and ball surface (Figure 1)	Excessive load	Ensure proper load condition
		Insufficient clearance	Ensure proper clearance and fitting
		Poor lubrication	Use the correct amount of appropriate lubricant
		Poor mounting	Check the accuracy of the shaft and housing, as well as the mounting method
	Flaking inclined toward the raceway (Figure 2)	Rust	Store and handle with care
		Poor mounting and shaft alignment (centering)	Mount and align (center) the bearings properly
		Shaft deflection	Select a bearing with a large clearance
Flaking at the symmetric position of the raceway	Poor accuracy of shaft and housing	Adjust the perpendicularity of the shaft and housing	
	Poor housing accuracy	Adjust the accuracy on the surface of the housing bore diameter	
Indentation	Ball-pitch indentations or dents on the raceway (Figure 3)	Impact load during mounting or when dropped	Handle with care
	Indentation on the raceway and ball surface	Excessive load when the bearing is stopped or during low-speed rotation	Check the static load
Seizure	Discoloration of raceway and ball surface	Intrusion of sand, metallic dust, etc.	Clean the shaft and housing, and check the sealing device
		Excessive load	Ensure proper clearance and fitting
		Insufficient clearance	Ensure proper clearance
		Poor lubrication	Use the correct amount of appropriate lubricant
Smearing	Softening and adhesion to raceway and ball surface (Figure 4)	Poor mounting	Check the mounting method and relevant components
		Sliding of balls	Apply proper preload
Electrolytic corrosion	Corrugated electrolytic corrosion of the raceway (Figure 5)	Poor lubrication	Use the correct amount of appropriate lubricant
Breakage	Cracked or chipped raceway surface (Figure 6)	Sparking resulting from an electric current passing through the bearing	Ground and/or insulate the bearing
		Excessive impact load	Apply appropriate load conditions
		Excessive interference	Ensure proper fitting
	Cracked or chipped balls	Developed flaking or seizure	Adjust the shaft and sleeve
		Excessive impact load	Check the mounting method and load condition
	Broken cage (Figure 7)	Excessive clearance during use	Check the fitting and bearing clearance
Moment load		Handle with care	
Impact due to high-speed and high-acceleration rotation		Check the rotation conditions	
Galling	Galling on the raceway and ball surface (Figure 8)	Inappropriate lubrication	Check the lubricant and lubrication methods
		Foreign matter has become entangled	Improve the sealing device
		Heavy acceleration at the start of use (ball slippage)	Improve the sealing device

Damage	Damage Symptoms	Cause	Remedy
Wear	Abnormal wear of raceway, balls, and cage (Figure 9)	Intrusion of foreign matter	Improve the sealing device
		Rust	Store and handle with care
		Poor lubrication	Use the correct amount of appropriate lubricant
	Galling wear on the fitting surface: creep (Figure 10)	Insufficient interference	Ensure proper fitting
		Insufficient sleeve fastening	Fasten the sleeve appropriately
	Red wear on the fitting surface: fretting (Figure 11)	Small clearance on fitting surface	Increase interference
Ball-pitch fretting on the raceway: false brinelling	Vibrations when the bearing is not used, such as during transportation	Fix the shaft and housing	
	Rocking movement with a small amplitude	Use oil as lubricant, and apply preload	
Rust and corrosion	Rust on the bearing surface and/or within the bearing	Poor storage conditions	Store and handle with care
		Condensation of moisture contained in air	Store and handle with care
	Rust on fitting surface (Figure 12)	Fretting	Increase interference
		Variable load	Apply oil on the fitting surface
	Corrosion	Intrusion of acid, alkali, or gas	Check the sealing device
		Chemical action of lubricant	Check the lubricant

Flaking



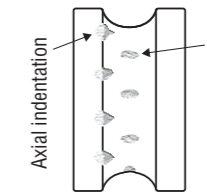
(Figure 1)

Poor mounting



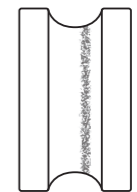
(Figure 2)

Indentation



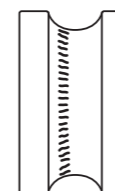
(Figure 3)

Smearing



(Figure 4)

Electrolytic corrosion



(Figure 5)

Crack



(Figure 6)

Broken cage



(Figure 7)

Galling



(Figure 8)

Ball scratches



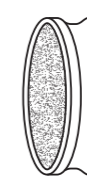
(Figure 9)

External creep



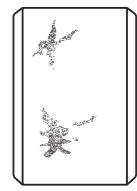
(Figure 10)

Fretting



(Figure 11)

Rust



(Figure 12)

Rolling Tracks and How Load is Applied

When a bearing rotates with a load applied, the rolling contact between the balls and the bearing rings will generate rolling tracks on the raceway surface of both inner and outer rings. The outline of rolling tracks and how the load is applied can be roughly summarized as shown in the eight figures below. Most of the damage to bearings at an early stage is caused by factors such as unexpected excessive load and mounting errors. Disassembling the bearing and looking at their rolling tracks will enable you to estimate the amount and direction of the load applied as well as the rotating rings, which will provide you with a clue on how to set appropriate load conditions.

Technical Contents

15 Damage to Bearings, and Its Causes and Remedies

Unidirectional radial load
(Inner ring: rotational, and outer ring: static)

Inner ring: The rolling track is observed at the center of the raceway over the entire circumference. The track has an even width throughout.

Outer ring: The rolling track is observed at the center of the raceway. The track is widest in the radial load direction, while it becomes narrower the farther it is from the load direction.

Unidirectional radial/axial loads
(combined load) (Inner ring: rotational, and outer ring: static)

Inner ring: The rolling track is deflected to the axial load direction, and is observed over the entire circumference of the raceway surface. The track has an even width throughout.

Outer ring: The rolling track is deflected to and is widest in the axial load direction. This may be observed either over the entire circumference, or just in some parts discontinuously.

Unidirectional radial load with radial preload
(or negative operating clearance)
(Inner ring: rotational, and outer ring: static)

Inner ring: The rolling track is observed at the center of the raceway over the entire circumference. The track has an even width throughout.

Outer ring: The rolling track can be observed at the center of the raceway either over the entire circumference, or just in some parts discontinuously. The track is widest in the radial load direction.

Axial load and moment load
(Inner ring: rotational, and outer ring: static)

Inner ring: The rolling track is deflected to the axial load direction, and is observed over the entire circumference of the raceway surface. The track has an even width throughout.

Outer ring: The rolling track is deflected to the axial load direction and is inclined diagonally, and is observed over the entire circumference of the raceway surface. The track has an even width throughout.

Unidirectional radial load
(Inner ring: static, and outer ring: rotational)

Inner ring: The rolling track is observed at the center of the raceway. The track gets widest in the radial load direction, while it becomes narrower the farther it is from the load direction.

Outer ring: The rolling track is observed at the center of the raceway over the entire circumference. The track has an even width throughout.

Moment load
(Inner ring: rotational, and outer ring: static)

Inner ring: The rolling track is observed at the center of the raceway over the entire circumference. The track has an even width throughout.

Outer ring: The rolling track is inclined diagonally with a fluctuating width.

Unidirectional axial load
(Inner ring: rotational, and/or outer ring: rotational)

Inner ring: The rolling track is deflected to the axial load direction, and is observed over the entire circumference of the raceway surface. The track has an even width throughout.

Outer ring: The rolling track is deflected to the axial load direction, and is observed over the entire circumference of the raceway surface. The track has an even width throughout.

When the outer ring is deformed to oval shape
(Inner ring: rotational, and outer ring: static)

Inner ring: The rolling track is observed at the center of the raceway over the entire circumference. The track has an even width throughout.

Outer ring: The rolling track is widest where the raceway is compressed. The length in the circumferential direction changes depending on the amount of deformation and the bearing's initial radial internal clearance.

16 > Main Lubricants

Main Oil Brands and Performances

Code	Brand	Manufacturer	Base oil	Flash point(°C)	Pour point(°C)	Kinematic viscosity (mm ² /s)	Specific gravity	Operating temperature (°C)	Features and applications
AF2	AeroShell Fluid 12 (standard oil)	Shell Lubricants Japan	Diester	220	-60 or less	11000(-54°C)、8.2(54°C)	0.93	-54 to +135	Low volatility, for aircraft gyroscopes and electronic devices
WL2	WINSOR L 245 X	Fuchs Lubritech	Diester	227	-65	13.02(40°C)	0.92	-50 to +80	Oxidation-resistant and wear-resistant, for electric motors and measuring instruments
KAZ	Krytox 143AZ	Chemours	Fluorinated	—	-55	22.8(40°C)、4.1(100°C)	1.91	-57 to +149	For home appliances, office equipment and aerospace applications, inert
PD8	Isoflex PDP38	Klüber Lubrication	Diester	200	-70	12.0(40°C)、3.2(100°C)	0.92	-65 to +100	Low temperature, for home appliances and precision equipment

Main Grease Brands and Performances

Code	Brand	Manufacturer	Base oil	Thickener	Dropping point (°C)	Worked penetration (25°C, 60 times)	Base oil kinematic viscosity (mm ² /s)	Specific gravity	Color	Operating temperature (°C)	Features and applications
SRL	Multemp SRL (standard grease)	Kyodo Yushi	Polyol Ester, Diester	Lithium	192	250	24.6(40°C)、4.9(100°C)	0.97	Light tan	-50 to +150	Low noise, long life, and low torque
PS2	Multemp PS No.2		Diester, Mineral	Lithium	190	275	15.3(40°C)、3.9(100°C)	0.91	White peach	-50 to +130	Low temperature, low torque, and low noise
SBM	Multemp SB-M		Synthetic hydrocarbon	Diurea	260	220	47.6(40°C)	0.85	Light tan	-40 to +200	Higher-temperature-resistant and longer-life version of Multemp SRL
RMS	Raremax Super		Mineral, Synthetic hydrocarbon	Diurea	255	260	10.5(100°C)	0.90	Light tan	-40 to +180	High temperature, low noise, oxidation-resistant, and corrosion-resistant, for motors
AV2	Shell Alvania Grease S2	Shell Lubricants Japan	Mineral	Lithium	181	283	131(40°C)、12.2(100°C)	0.90	Amber	-25 to +120	General multipurpose
AV3	Shell Alvania Grease S3		Mineral	Lithium	182	242	131(40°C)、12.2(100°C)	0.90	Amber	-20 to +135	General multipurpose
AG3	AeroShell Grease 33		Synthetic hydrocarbon, Ester	Lithium	216	297	14.2(40°C)、3.4(100°C)	1.00	Green	-73 to +121	Oxidation-resistant, corrosion-resistant and load-resistant
M3L	Molykote 33L Grease	DuPont Toray Specialty Materials	Silicone	Lithium	210	320	100(25°C)	1.00	White	-73 to +180	Oxidation-resistant, wide temperature range, low temperature, and water-resistant
M3M	Molykote 33M Grease		Silicone	Lithium	210	280	100(25°C)	1.00	White	-73 to +180	Oxidation-resistant, wide temperature range, low temperature, and water-resistant
M4M	Molykote 44M Grease		Silicone	Lithium	204	260	125(25°C)	1.00	White	-40 to +200	Low evaporation, oxidation-resistant, wide temperature range, low temperature, and water-resistant
G45	Molykote G-4500 FM Multi-Purpose Synthetic Grease		PAO	Aluminum complex	270	280	100(40°C)、14.4(100°C)	0.84	White	-40 to +150	Wide temperature range, for food machinery (NSF H1)
RL2	Cassida Grease RLS2	Fuchs Lubritech	Synthetic	Aluminum complex	240	280	150(40°C)、18(100°C)	0.88	White	-35 to +120	For food machinery (NSF H1)
GHY	Asonic GHY 72	Klüber Lubrication	Ester	Polyurea	250	265	72(40°C)、9.5(100°C)	0.95	Brown-yellow	-40 to +180	High temperature, low noise, and high speed
GLY	Asonic GLY 32		Synthetic hydrocarbon, Ester	Lithium	190	280	25(40°C)、5(100°C)	0.94	Light brown	-50 to +140	Low temperature, low torque, low noise, and high speed
HQ7	Asonic HQ 72-102		Ester	Polyurea	240	265	100(40°C)、12(100°C)	0.97	Light brown	-40 to +180	High temperature, low noise, and water-resistant

Code	Brand	Manufacturer	Base oil	Thickener	Dropping point (°C)	Worked penetration (25°C, 60 times)	Base oil kinematic viscosity (mm ² /s)	Specific gravity	Color	Operating temperature (°C)	Features and applications
B52	Isoflex TOPAS NB 52	Klüber Lubrication	Synthetic hydrocarbon	Barium	240	280	30(40°C)、5.9(100°C)	0.96	Light brown	-50 to +120	Load-resistant, heat-resistant, water-resistant, high speed, and supports electrical contact
L8A	Isoflex LDS 18 Special A		Ester, Mineral	Lithium	190	280	15.0(40°C)、3.5(100°C)	0.88	Yellow	-50 to +120	Low temperature, low torque, biodegradable, and high speed (dmn100×10 ⁴)
SL8	Isoflex Super LDS 18-R		Ester, Mineral	Lithium	190	280	15.0(40°C)、3.5(100°C)	0.90	Yellow	-50 to +120	Low temperature, low torque, and high speed (dmn100×10 ⁴)
NB5	Isoflex NBU 15		Synthetic hydrocarbon, Mineral, Ester	Barium	220	280	21(40°C)、4.5(100°C)	0.99	Light brown	-40 to +130	Load-resistant, wear-resistant, water-resistant, and high speed, for spindles
NB2	Staburags NBU 12		Mineral	Barium	220	260	220(40°C)、19(100°C)	0.99	Light tan	-15 to +150	Load-resistant, water-resistant, and chemical-resistant, for food machinery (NSF H2)
NB3	Staburags NBU 12/300 KP		Mineral	Barium	220	300	225(40°C)、19(100°C)	0.97	Light tan	-20 to +130	Load-resistant, water-resistant, and chemical-resistant
IMI	Barrierta IMI		PFPE	PTFE	—	280	200(40°C)、22(100°C)	1.95	White	-45 to +220	High temperature, low torque, high speed, and supports electrical contact
L55	Barrierta L55/2 H1		PFPE	PTFE	—	280	420(40°C)、40(100°C)	1.96	White	-40 to +260	High temperature, oxidation-resistant, and chemical-resistant, for food machinery (NSF H1)
E55	Barrierta JFE 552		PFPE	PTFE	—	280	NKL apparent viscosity: S	1.90	White	-35 to +260	High temperature, oxidation-resistant, and chemical-resistant
UH6	Klubersynth UH1 64-62		Synthetic hydrocarbon, Ester	Silica	—	280	65(40°C)、10(100°C)	0.92	Light brown	-40 to +140	Load-resistant, wear-resistant, and water-resistant, for food machinery (NSF H1)
K24	Krytox 240AC	Chemours	PFPE	PTFE	—	280	270(38°C)、26(99°C)	1.93	White	-34 to +288	High temperature, oxidation-resistant, and chemical-resistant, for food machinery (NSF H1)
K2Z	Krytox 240AZ		PFPE	PTFE	—	280	24.7(38°C)、4.2(99°C)	1.89	White	-57 to +149	Oxidation-resistant, chemical-resistant, for food machinery (NSF H1)
MG2	Mobilgrease 28	ExxonMobil	PAO	Organog Clay	307	293	29.3(40°C)、5.7(100°C)	0.95	Dark red	-54 to +177	Wide temperature range, wear-resistant
B32	Beacon 325J		Synthetic	Lithium	194	262	11.54(40°C)、3.204(100°C)	0.94	Beige	-50 to +120	Low temperature, low torque, low noise, and long life
PEM	Polyrex EM (Polyree EM)		Mineral	Polyurea	260	285	115(40°C)、12.2(100°C)	0.88	Blue	-20 to +180	Low-noise, for electric motors
CGA	RHEOLUBE 374C	Nye Lubricants	PAO	Lithium	260	193	60.7(40°C)、9.5(100°C)	0.87	Yellow-brown	-40 to +150	Wide temperature range, and high speed
AFF	AFF Grease	THK	Synthetic	Lithium	220	315	100(40°C)	0.98	Tan	-40 to +120	Anti-fretting and low-dust grease
NBF	NIGACE W (BF)	Nippon Grease	Mineral, Synthetic	Urea	250	255	—	0.88	Light tan	-30 to +150	Low noise and long life
RYC	ROYCO 22CF	LANXESS	PAO	Inorganic gel	232	283	—	0.88	Dark brown	-54 to +177	Wide temperature range, water-resistant and load-resistant

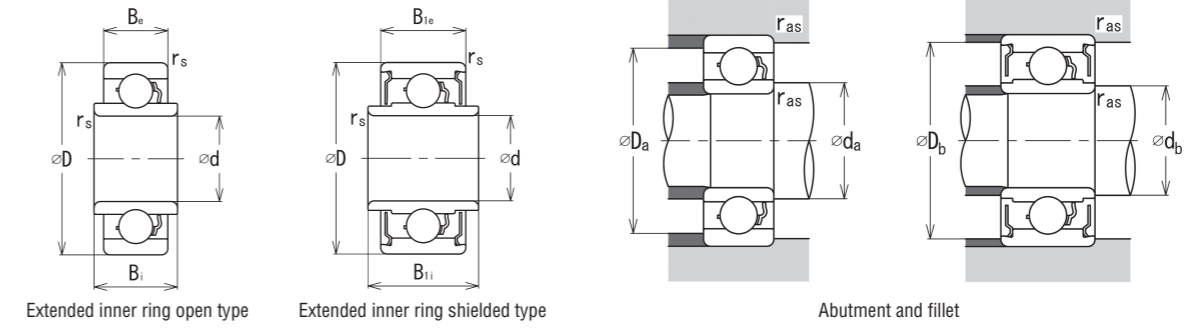
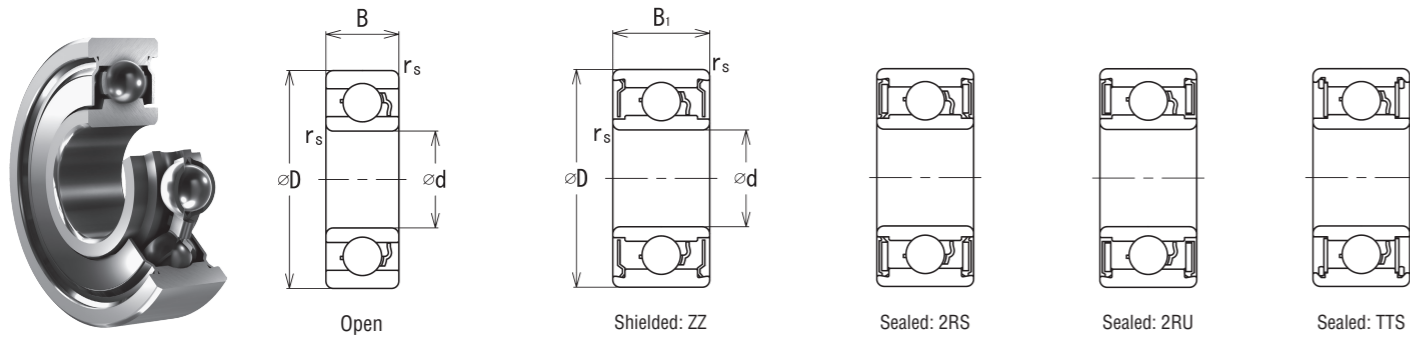
Note: When you are planning to use a bearing filled with an NSF H1 or H2 registered lubricant for food machinery, please consult with us because an additional cleanliness management procedure will be required in the assembly process.

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Inch-series bearings [Stainless-steel]



Dimension

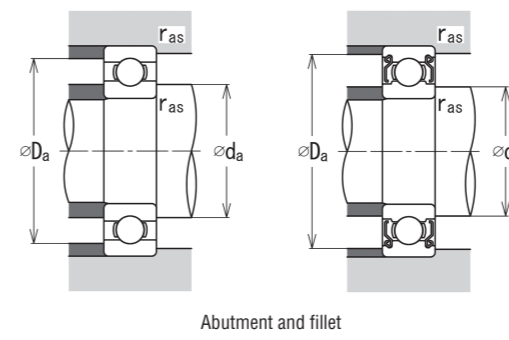
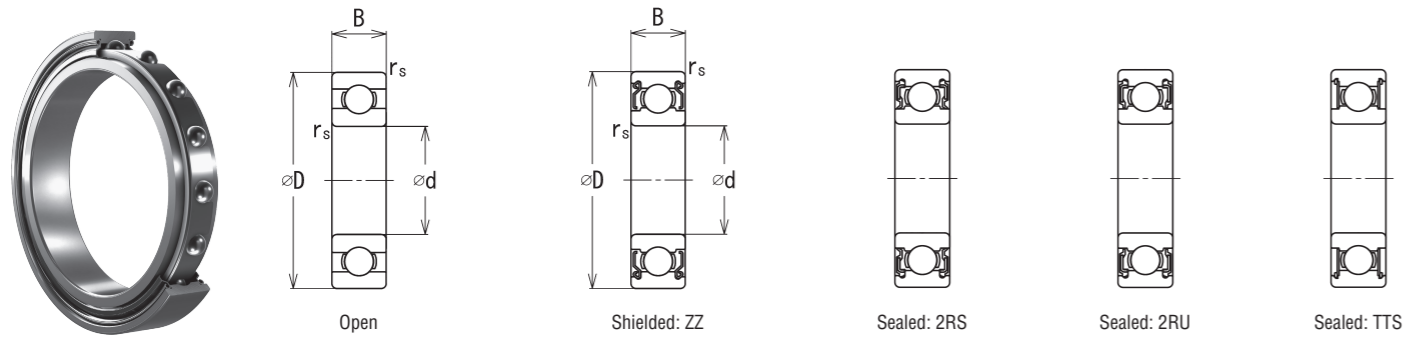
Inch-series bearings [Stainless-steel]

Bore diameter d		Outer diameter D		Inner ring width				Outer ring width				Chamfer rs (min)		Bearing number					
				Open B, B1		Shielded, Sealed B1, B11		Open B, B2		Shielded, Sealed B1, B12				Open	2 Shields ⁽²⁾		2 Seals ⁽²⁾		
				mm	inch	mm	inch	mm	inch	mm	inch				mm	inch	2RS	2RU	TTS
6.350	0.2500	15.875	0.6250	4.978	0.1960	4.978	0.1960	4.978	0.1960	4.978	0.1960	0.30	0.0118	SR4 ⁽¹⁾	SR4ZZ	2RS	2RU	—	
		15.875	0.6250	—	—	4.978	0.1960	—	—	4.978	0.1960	0.30	0.0118	—	—	—	—	TTS	
		15.875	0.6250	5.771	0.2272	5.771	0.2272	4.978	0.1960	4.978	0.1960	0.30	0.0118	SRW4 ⁽¹⁾	SRW4ZZ	2RS	—	—	
7.938	0.3125	19.050	0.7500	5.558	0.2188	7.142	0.2812	5.558	0.2188	7.142	0.2812	0.40	0.0157	SR4A	SR4AZZ	2RS	2RU	TTS	
		12.700	0.5000	3.967	0.1562	3.967	0.1562	3.967	0.1562	3.967	0.1562	0.15	0.0059	SR1810 ⁽¹⁾	SR1810ZZS	—	—	TTS	
		12.700	0.5000	4.762	0.1875	4.762	0.1875	3.967	0.1562	3.967	0.1562	0.15	0.0059	SRW1810 ⁽¹⁾	SRW1810ZZS	—	—	TTS	
9.525	0.3750	22.225	0.8750	5.558	0.2188	7.142	0.2812	5.558	0.2188	7.142	0.2812	0.40	0.0157	SR6	SR6ZZ	2RS	2RU	—	
		22.225	0.8750	—	—	7.142	0.2812	—	—	7.142	0.2812	0.40	0.0157	—	—	—	—	TTS	
12.700	0.5000	28.575	1.1250	6.350	0.2500	7.938	0.3125	6.350	0.2500	7.938	0.3125	0.40	0.0157	SR8	SR8ZZ	2RS	2RU	—	
15.875	0.6250	34.925	1.3750	7.142	0.2812	8.733	0.3438	7.142	0.2812	8.733	0.3438	0.80	0.0315	SR10	SR10ZZ	—	—	—	
		34.925	1.3750	—	—	8.733	0.3438	—	—	8.733	0.3438	0.80	0.0315	—	—	2RS	2RU	—	
19.050	0.7500	41.275	1.6250	7.938	0.3125	—	—	7.938	0.3125	—	—	0.80	0.0315	SR12	—	—	—	—	
		41.275	1.6250	—	—	11.113	0.4375	—	—	11.113	0.4375	0.80	0.0315	—	SR12ZZ	2RS	—	—	
12.700	0.5000	22.225	0.8750	5.558	0.2188	7.142	0.2812	5.558	0.2188	7.142	0.2812	0.40	0.0157	SR6-5	SR6-5ZZS	—	—	—	

- (1) Open bearings have shield/seal grooves.
- (2) Single-shielded/single-sealed bearings are also available; suffix Z, RS, RU or TS.
- (3) Applicable only for open, single Z, ZZ, single RU and 2RU types in inner ring rotating conditions.
Limiting speeds for the contact rubber seal(s) types can be lower than the above-mentioned values, so please check the detailed values per item on "products" section of our website.
- (4) Some items are also available with the TW cage. Please contact us for details.

Load rating		Limiting speed ⁽³⁾		Cage type ⁽⁴⁾	Ball		Abutment and fillet dimensions								Mass (Ref.)		
Cr	Cor	Grease	Oil		Size	Qty.	Open				Shielded, Sealed				ras (max)	Open	2 Shields
N			min ⁻¹		mm	pcs.	da (min)	da (max)	Da (min)	Da (max)	db (min)	db (max)	D2 (min)	D2 (max)		mm	g
1 260	493	42 000	50 000	J	2.381	8	8.00	8.30	13.90	14.30	8.00	8.30	13.90	14.30	0.30	3.82	4.15
1 260	493	34 000	34 000	J	2.381	8	—	—	—	—	8.00	8.30	13.50	13.90	0.30	—	4.15
1 260	493	42 000	50 000	J	2.381	8	8.00	8.30	13.90	14.30	8.00	8.30	13.90	14.30	0.30	3.97	4.29
1 990	711	38 000	45 000	J	3.500	6	8.90	10.00	15.10	16.60	8.40	8.40	16.60	17.10	0.40	7.34	8.85
460	221	45 000	53 000	W	1.200	12	8.90	8.90	11.60	11.90	8.90	8.90	11.60	11.90	0.15	1.40	1.48
460	221	45 000	53 000	W	1.200	12	8.90	8.90	11.60	11.90	8.90	8.90	11.60	11.90	0.15	1.47	1.56
2 830	1 130	31 000	37 000	J	3.969	7	12.10	12.70	18.80	19.80	11.60	11.80	20.00	20.10	0.40	8.64	10.6
2 830	1 130	24 000	24 000	J	3.969	7	—	—	—	—	11.60	11.80	19.80	20.30	0.40	—	10.1
4 350	1 910	25 000	30 000	J	4.762	8	15.50	16.50	24.00	26.50	15.00	15.50	25.50	26.50	0.40	17.0	20.2
5 100	2 610	20 000	24 000	RJ	4.762	10	20.50	23.00	30.50	31.50	20.50	23.00	31.50	31.50	0.80	29.4	35.4
5 100	2 610	20 000	24 000	RJ	4.762	10	—	—	—	—	20.50	21.00	31.00	31.50	0.80	—	35.3
6 730	3 560	17 000	21 000	RJ	5.556	10	24.00	27.00	35.00	37.00	—	—	—	—	0.80	45.9	—
7 980	4 050	17 000	20 000	RJ	6.350	9	—	—	—	—	24.00	27.50	37.50	38.00	0.80	—	59.7
1 630	834	30 000	36 000	J	2.381	12	14.50	14.50	18.50	20.00	14.50	14.50	19.50	20.00	0.40	7.60	9.69

Extra-thin-section bearings [SUJ2]



Dimension

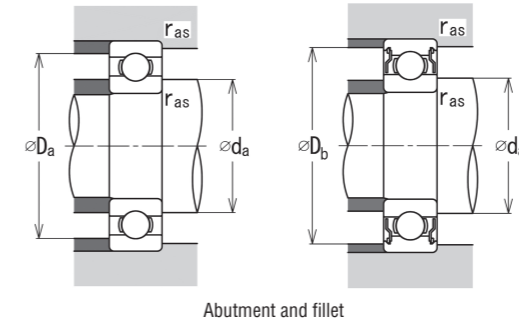
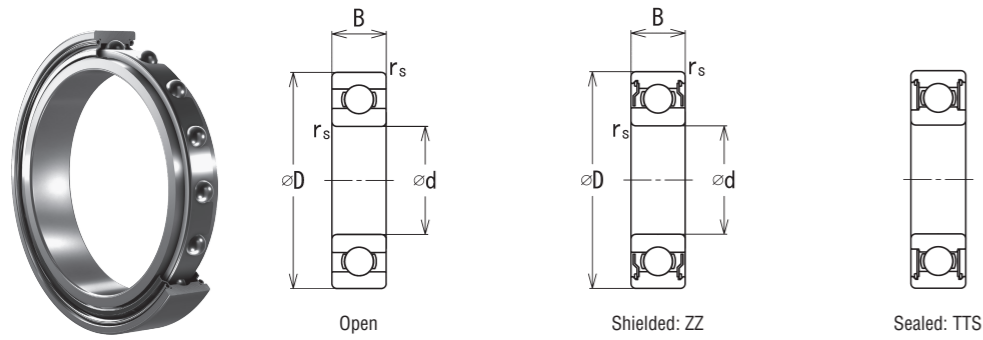
Extra-thin-section bearings [SUJ2]

Bore diameter d		Outer diameter D		Width B		Chamfer rs (min)		Bearing number					Load rating		Limiting speed ⁽³⁾		Cage type ⁽⁴⁾
								Open	2 Shields ⁽²⁾	2 Seals ⁽²⁾			Cr	Cor	Grease	Oil	
mm	inch	mm	inch	mm	inch	mm	inch			2RS	2RU	TTS	N				
50	1.9685	72	2.8346	12	0.4724	0.60	0.0236	6910 ⁽¹⁾	6910ZZ	2RS	2RU	—	14 500	11 700	9 000	11 000	RJ
55	2.1654	72	2.8346	9	0.3543	0.30	0.0118	6811 ⁽¹⁾	6811ZZ	2RS	2RU	—	8 800	8 080	8 600	10 000	RJ
								6911 ⁽¹⁾	6911ZZ	2RS	2RU	—	16 600	14 100	8 100	9 600	RJ
60	2.3622	78	3.0709	10	0.3937	0.30	0.0118	6812 ⁽¹⁾	6812ZZ	2RS	2RU	—	11 500	10 600	7 900	9 400	RJ
								6912 ⁽¹⁾	6912ZZ	2RS	2RU	—	20 200	17 300	7 500	8 900	RJ
65	2.5591	85	3.3465	10	0.3937	0.60	0.0236	6813 ⁽¹⁾	6813ZZ	2RS	—	—	11 900	11 500	7 300	8 600	RJ
								6913 ⁽¹⁾	6913ZZ	2RS	—	—	17 300	16 000	7 000	8 300	RJ
70	2.7559	90	3.5433	10	0.3937	0.60	0.0236	6814 ⁽¹⁾	6814ZZ	2RS	2RU	—	11 600	11 800	6 800	8 100	RJ
								6914 ⁽¹⁾	6914ZZ	2RS	—	—	23 700	21 100	6 400	7 600	RJ
75	2.9528	95	3.7402	10	0.3937	0.60	0.0236	6815 ⁽¹⁾	6815ZZ	2RS	—	—	12 300	12 800	6 400	7 600	RJ
								6915 ⁽¹⁾	6915ZZ	2RS	—	—	24 000	22 600	6 000	7 100	RJ
80	3.1496	100	3.9370	10	0.3937	0.60	0.0236	6816 ⁽¹⁾	6816ZZ	2RS	2RU	—	12 600	13 300	6 000	7 100	RJ
								6916 ⁽¹⁾	6916ZZ	2RS	—	—	24 800	23 900	5 700	6 700	RJ
85	3.3465	110	4.3307	13	0.5118	1.00	0.0394	6817 ⁽¹⁾	6817ZZ	2RS	—	—	18 700	19 000	5 600	6 600	RJ
								6917 ⁽¹⁾	6917ZZ	2RS	—	—	31 900	29 600	5 300	6 200	RJ
90	3.5433	115	4.5276	13	0.5118	1.00	0.0394	6818 ⁽¹⁾	6818ZZ	2RS	—	—	18 300	19 500	5 300	6 200	RJ
								6918 ⁽¹⁾	—	2RS	—	—	32 400	31 600	5 000	5 900	RJ
95	3.7402	120	4.7244	13	0.5118	1.00	0.0394	6819 ⁽¹⁾	—	—	2RU	—	18 800	20 300	5 000	5 900	RJ

Ball		Abutment and fillet dimensions					Mass (Ref.)	
Size	Qty.	da (min)	da (max)	Da (min)	Da (max)	ras (max)	Open	2 Shields
mm	pcs.	mm					g	
6.747	16	54.00	56.50	68.00	68.50	0.60	123	131
4.762	22	57.00	60.00	69.00	70.00	0.30	74.7	78.3
7.144	17	60.00	62.50	75.50	75.50	1.00	168	177
5.556	21	62.00	65.00	75.00	76.00	0.30	93.9	99.4
7.938	17	65.00	67.50	80.50	80.50	1.00	180	186
5.556	23	69.00	71.00	81.00	81.50	0.60	118	125
7.144	19	70.00	72.50	85.00	85.00	1.00	198	208
5.556	24	74.00	76.00	86.00	86.50	0.60	127	135
8.731	17	75.00	79.00	94.00	95.00	1.00	320	335
5.556	26	79.00	81.00	91.00	91.50	0.60	135	143
8.731	18	80.00	84.00	99.00	100.00	1.00	342	357
5.556	27	84.00	86.00	96.00	96.50	0.60	144	152
8.731	19	85.00	89.00	103.50	105.00	1.00	364	379
7.144	23	90.00	92.50	105.50	105.50	1.00	244	258
10.319	17	91.50	96.00	113.00	113.50	1.00	508	526
7.144	24	95.00	97.50	110.00	110.00	1.00	251	267
10.319	18	96.50	101.00	118.50	119.50	1.00	537	561
7.144	25	100.00	102.50	115.50	115.50	1.00	267	284

(1) Open bearings have shield/seal grooves.
 (2) Single-shielded/single-sealed bearings are also available; suffix Z, RS, RU or TS.
 (3) Applicable only for open, single Z, ZZ, single RU and 2RU types in inner ring rotating conditions.
 Limiting speeds for the contact rubber seal(s) types can be lower than the above-mentioned values, so please check the detailed values per item on "products" section of our website.
 (4) Some items are also available with the TW cage. Please contact us for details.

Extra-thin-section ET, ER bearings



ET series (Metric series) SUJ2

Bore diameter d		Outer diameter D		Width B		Chamfer r _s (min)		Bearing number			Load rating		Limiting speed ⁽³⁾		Cage type
mm	inch	mm	inch	mm	inch	mm	inch	Open	2 Shields ⁽²⁾	2 Seals ⁽²⁾	Cr	Cor	Grease	Oil	
								TTS			N		min ⁻¹		
15	0.5906	20	0.7874	3.5	0.1378	0.15	0.0059	ET2015	—	—	943	583	11 000	13 000	W
		21	0.8268	3.5	0.1378	0.15	0.0059	ET2115	—	—	937	581	11 000	13 000	W
16	0.6299	22	0.8661	4	0.1575	0.15	0.0059	ET2216	ET2216ZZS	—	971	620	10 000	12 000	W
20	0.7874	25	0.9843	4	0.1575	0.15	0.0059	ET2520 ⁽¹⁾	ET2520ZZS	—	1 010	691	8 500	10 000	W

ER series (Inch series) SUJ2

Bore diameter d		Outer diameter D		Width B		Chamfer r _s (min)		Bearing number			Load rating		Limiting speed ⁽³⁾		Cage type
mm	inch	mm	inch	mm	inch	mm	inch	Open	2 Shields ⁽²⁾	2 Seals ⁽²⁾	Cr	Cor	Grease	Oil	
								TTS			N		min ⁻¹		
9.525	0.3750	15.875	0.6250	3.967	0.1562	0.25	0.0098	ER1038 ⁽¹⁾	ER1038ZZS	—	857	435	15 000	17 500	W
12.700	0.5000	19.050	0.7500	3.967	0.1562	0.25	0.0098	ER1212 ⁽¹⁾	ER1212ZZS	TTS	919	537	12 000	14 000	W
19.05	0.7500	25.400	1.0000	3.967	0.1562	0.25	0.0098	ER1634 ⁽¹⁾	ER1634ZZS	—	1 010	691	8 500	10 000	W

SET series (Metric series) Stainless-steel

Bore diameter d		Outer diameter D		Width B		Chamfer r _s (min)		Bearing number			Load rating		Limiting speed ⁽³⁾		Cage type
mm	inch	mm	inch	mm	inch	mm	inch	Open	2 Shields ⁽²⁾	2 Seals ⁽²⁾	Cr	Cor	Grease	Oil	
								TTS			N		min ⁻¹		
20	0.7874	25	0.9843	4	0.1575	0.15	0.0059	SET2520 ⁽¹⁾	SET2520ZZS	—	861	553	8 500	10 000	W

SER (Inch series) Stainless-steel

Bore diameter d		Outer diameter D		Width B		Chamfer r _s (min)		Bearing number			Load rating		Limiting speed ⁽³⁾		Cage type
mm	inch	mm	inch	mm	inch	mm	inch	Open	2 Shields ⁽²⁾	2 Seals ⁽²⁾	Cr	Cor	Grease	Oil	
								TTS			N		min ⁻¹		
9.525	0.3750	15.875	0.6250	3.967	0.1562	0.25	0.0098	SER1038 ⁽¹⁾	SER1038ZZS	TTS	729	348	15 000	17 500	W
12.700	0.5000	19.050	0.7500	3.967	0.1562	0.25	0.0098	SER1212 ⁽¹⁾	SER1212ZZS	TTS	781	429	12 000	14 000	W
15.875	0.6250	22.225	0.8750	3.967	0.1562	0.25	0.0098	SER1458 ⁽¹⁾	SER1458ZZS	—	825	496	10 000	12 000	W
19.050	0.7500	25.400	1.0000	3.967	0.1562	0.25	0.0098	SER1634 ⁽¹⁾	SER1634ZZS	—	861	553	8 500	10 000	W

(1) Open bearings have shield/seal grooves.

(2) Single-shielded/single-sealed bearings are also available; suffix ZS or TS.

(3) Applicable only for open, single ZS and ZZS bearings in inner ring rotating conditions.

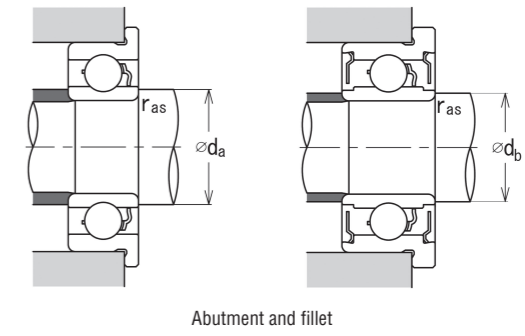
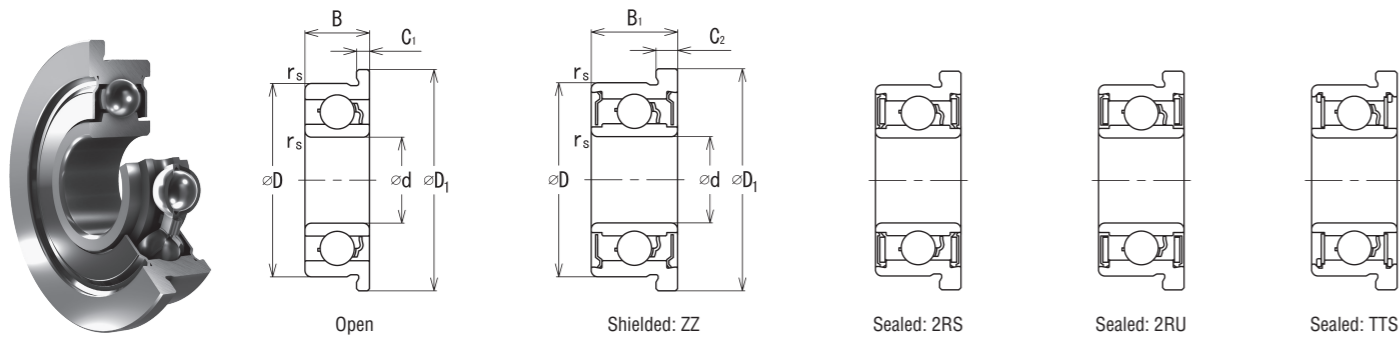
Ball		Abutment and fillet dimensions						Mass (Ref.)		
Size	Qty.	d _a (min)	d _a (max)	Open		Shielded, Sealed		r _{as} (max)	Open	2 Shields
mm	pcs.	mm		D _a (min)	D _a (max)	D _b (min)	D _b (max)	mm	g	
1.588	14	16.00	16.00	19.00	19.50	—	—	0.15	2.14	—
1.588	14	16.00	16.50	19.50	20.00	—	—	0.15	3.04	—
1.588	15	17.00	17.50	20.50	21.00	21.00	21.50	0.15	3.66	3.69
1.588	17	21.00	21.00	24.50	24.50	24.50	24.50	0.15	2.96	3.30

Ball		Abutment and fillet dimensions						Mass (Ref.)		
Size	Qty.	d _a (min)	d _a (max)	Open		Shielded, Sealed		r _{as} (max)	Open	2 Shields
mm	pcs.	mm		D _a (min)	D _a (max)	D _b (min)	D _b (max)	mm	g	
1.588	11	11.10	11.20	14.30	14.30	14.30	14.30	0.25	2.40	2.60
1.588	13	14.00	14.00	17.50	18.00	17.50	18.00	0.25	3.01	3.26
1.588	17	21.00	21.00	24.50	24.50	24.50	24.50	0.25	4.22	4.56

Ball		Abutment and fillet dimensions						Mass (Ref.)		
Size	Qty.	d _a (min)	d _a (max)	Open		Shielded, Sealed		r _{as} (max)	Open	2 Shields
mm	pcs.	mm		D _a (min)	D _a (max)	D _b (min)	D _b (max)	mm	g	
1.588	17	21.00	21.00	24.50	24.50	24.50	24.50	0.15	2.92	3.26

Ball		Abutment and fillet dimensions						Mass (Ref.)		
Size	Qty.	d _a (min)	d _a (max)	Open		Shielded, Sealed		r _{as} (max)	Open	2 Shields
mm	pcs.	mm		D _a (min)	D _a (max)	D _b (min)	D _b (max)	mm	g	
1.588	11	11.10	11.20	14.30	14.30	14.30	14.30	0.25	2.37	2.57
1.588	13	14.00	14.00	17.50	18.00	17.50	18.00	0.25	2.98	3.22
1.588	15	17.50	17.50	21.00	21.00	21.00	21.00	0.25	3.60	3.89
1.588	17	21.00	21.00	24.50	24.50	24.50	24.50	0.25	4.17	4.51

Flanged inch-series bearings [SUJ2]



Dimension

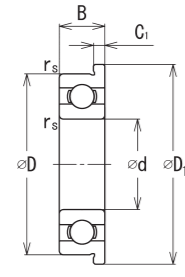
Flanged inch-series bearings [SUJ2]

Bore diameter d		Outer diameter D		Width				Flange outer diameter D ₁		Flange width				Chamfer r _s (min)		Bearing number	
				Open B		Shielded, Sealed B ₁				Open C ₁		Shielded, Sealed C ₂				Open	2 Shields ⁽²⁾
mm	inch	mm	inch	mm	inch	mm	inch	mm	inch	mm	inch	mm	inch	mm	inch		
2.380	0.0937	4.762	0.1875	1.588	0.0625	—	—	5.944	0.2340	0.457	0.0180	—	—	0.10	0.0039	FR133	—
3.175	0.1250	6.350	0.2500	—	—	2.779	0.1094	7.518	0.2960	—	—	0.787	0.0310	0.10	0.0039	—	FR144ZZ
		7.938	0.3125	—	—	3.571	0.1406	9.119	0.3590	—	—	0.787	0.0310	0.10	0.0039	—	FR2-5ZZ
		9.525	0.3750	3.967	0.1562	3.967	0.1562	11.176	0.4400	0.762	0.0300	0.762	0.0300	0.30	0.0118	FR2⁽¹⁾	FR2ZZ
3.967	0.1562	7.938	0.3125	—	—	3.175	0.1250	9.119	0.3590	—	—	0.914	0.0360	0.10	0.0039	—	FR155ZZS
4.762	0.1875	12.700	0.5000	4.978	0.1960	4.978	0.1960	14.351	0.5650	1.067	0.0420	1.067	0.0420	0.30	0.0118	FR3	FR3ZZ
6.350	0.2500	9.525	0.3750	—	—	3.175	0.1250	10.719	0.4220	—	—	0.914	0.0360	0.10	0.0039	—	FR168ZZ
		12.700	0.5000	—	—	4.762	0.1875	13.894	0.5470	—	—	1.143	0.0450	0.15	0.0059	—	FR188ZZ
		15.875	0.6250	4.978	0.1960	4.978	0.1960	17.526	0.6900	1.067	0.0420	1.067	0.0420	0.30	0.0118	FR4⁽¹⁾	FR4ZZ
7.938	0.3125	12.700	0.5000	3.967	0.1562	3.967	0.1562	13.894	0.5470	0.787	0.0310	0.787	0.0310	0.15	0.0059	FR1810⁽¹⁾	FR1810ZZS
9.525	0.3750	22.225	0.8750	5.558	0.2188	7.142	0.2812	24.613	0.9690	1.575	0.0620	1.575	0.0620	0.40	0.0157	FR6	FR6ZZ
12.700	0.5000	28.575	1.1250	6.350	0.2500	7.938	0.3125	31.120	1.2252	1.575	0.0620	1.575	0.0620	0.40	0.0157	FR8	FR8ZZ
15.875	0.6250	34.925	1.3750	—	—	8.733	0.3438	37.846	1.4900	—	—	1.745	0.0687	0.80	0.0315	—	FR10ZZ

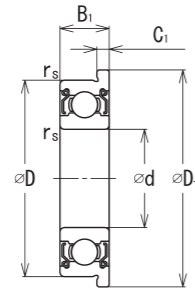
(1) Open bearings have shield/seal grooves.
 (2) Single-shielded/single-sealed bearings are also available; suffix Z, RS, RU or TS. (shielded/sealed at flanged side unless otherwise requested)
 (3) Applicable only for open, single Z, ZZ, single RU and 2RU types in inner ring rotating conditions. Limiting speeds for the contact rubber seal(s) types can be lower than the above-mentioned values, so please check the detailed values per item on "products" section of our website.
 (4) Some items are also available with the TW cage. Please contact us for details.

Bearing number	Load rating		Limiting speed ⁽³⁾		Cage type ⁽⁴⁾	Ball		Abutment and fillet dimensions				Mass (Ref.)				
	2 Seals ⁽²⁾		Cr	Cor		Grease	Oil	Size	Qty.	Open		Shielded, Sealed		r _{as} (max)	Open	2 Shields
	2RS	2RU	TTS	N						min ⁻¹	d _a (min)	d _a (max)	d _b (min)			
—	—	—	189	60	90 000	106 000	W	0.800	7	2.90	2.90	—	—	0.10	0.13	—
—	—	—	284	95	77 000	91 000	W	1.000	7	—	—	3.80	3.80	0.10	—	0.36
—	—	—	559	179	70 000	82 000	W	1.588	6	—	—	4.00	4.30	0.10	—	0.75
—	—	—	633	218	66 000	78 000	J	1.588	7	4.70	4.70	4.70	4.70	0.30	1.39	1.46
—	—	—	360	149	64 000	76 000	W	1.000	10	—	—	4.80	5.40	0.10	—	0.69
2RS	—	—	1 300	485	51 000	60 000	J	2.381	7	6.80	6.90	6.40	6.40	0.30	2.93	2.91
—	—	—	373	172	55 000	65 000	W	1.000	11	—	—	7.00	7.00	0.10	—	0.67
—	—	—	1 080	438	48 000	56 000	J	2.000	8	—	—	7.20	7.30	0.15	—	2.24
2RS	2RU	—	1 480	617	42 000	50 000	J	2.381	8	8.00	8.30	8.00	8.30	0.30	4.26	4.58
—	—	TTS	541	276	45 000	53 000	W	1.200	12	8.90	8.90	8.90	8.90	0.15	1.56	1.65
2RS	2RU	—	3 330	1 410	31 000	37 000	J	3.969	7	12.10	12.70	11.60	11.80	0.40	9.85	11.8
2RS	2RU	—	5 110	2 390	25 000	30 000	J	4.762	8	15.50	16.50	15.00	15.50	0.40	18.7	21.8
—	—	—	6 000	3 270	20 000	24 000	RJ	4.762	10	—	—	20.50	23.00	0.80	—	38.5

Flanged extra-thin-section bearings [Stainless-steel]



Open



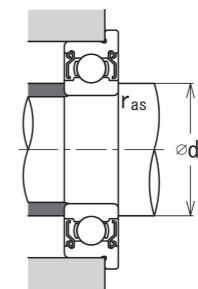
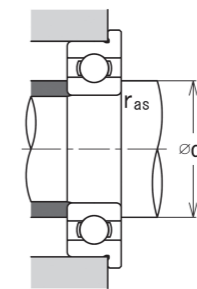
Shielded: ZZ



Sealed: 2RS



Sealed: 2RU



Abutment and fillet

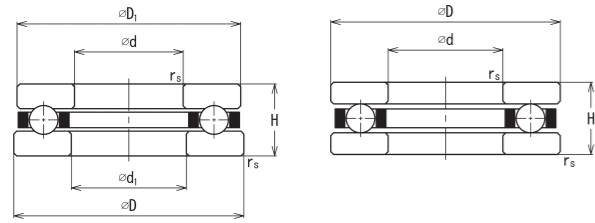
Bore diameter d		Outer diameter D		Width				Flange outer diameter D ₁		Flange width C ₁		Chamfer r _s (min)		Bearing number			
				Open B		Shielded, Sealed B ₁								Open	2 Shields ⁽²⁾		2 Shields ⁽²⁾
mm	inch	mm	inch	mm	inch	mm	inch	mm	inch	mm	inch	mm	inch				2RS
10	0.3937	15	0.5906	3	0.1181	4	0.1575	16.5	0.6496	0.800	0.0315	0.15	0.0059	F6700H	F6700HZZ	2RS	—
				5	0.1969	5	0.1969	21	0.8268	1.000	0.0394	0.30	0.0118	F6800H⁽¹⁾	F6800HZZ	2RS	2RU
				7	0.2756	7	0.2756	21	0.8268	1.500	0.0591	0.30	0.0118	F63800H⁽¹⁾	F63800HZZ	2RS	2RU
12	0.4724	18	0.7087	4	0.1575	4	0.1575	19.5	0.7677	0.800	0.0315	0.20	0.0079	F6701H⁽¹⁾	F6701HZZ	2RS	—
				5	0.1969	5	0.1969	23	0.9055	1.100	0.0433	0.30	0.0118	F6801H⁽¹⁾	F6801HZZ	2RS	2RU
				6	0.2362	6	0.2362	26.5	1.0433	1.500	0.0591	0.30	0.0118	F6901H⁽¹⁾	F6901HZZ	2RS	2RU
15	0.5906	21	0.8268	4	0.1575	4	0.1575	22.5	0.8858	0.800	0.0315	0.20	0.0079	F6702H⁽¹⁾	F6702HZZ	2RS	—
				5	0.1969	5	0.1969	26	1.0236	1.100	0.0433	0.30	0.0118	F6802H⁽¹⁾	F6802HZZ	2RS	2RU
				7	0.2756	—	—	26	1.0236	1.500	0.0591	0.30	0.0118	F63802H⁽¹⁾	—	—	—
				7	0.2756	7	0.2756	30.5	1.2008	1.500	0.0591	0.30	0.0118	F6902H⁽¹⁾	F6902HZZ	2RS	2RU

Load rating		Limiting speed ⁽³⁾		Cage type ⁽⁴⁾	Ball		Abutment and fillet dimensions			Mass (Ref.)	
Cr	Cor	Grease	Oil		Size	Qty.	d _s (min)	d _s (max)	r _{as} (max)	Open	2 Shields
N		min ⁻¹			mm	pcs.	mm			g	
729	348	15 000	17 000	W	1.588	11	11.00	11.00	0.15	1.54	1.96
1 460	672	34 000	40 000	J	2.381	10	11.50	11.50	0.30	5.24	5.53
1 460	672	34 000	40 000	J	2.381	10	11.50	11.50	0.30	7.40	7.68
2 290	1 020	31 000	37 000	J	3.175	9	12.00	13.00	0.30	9.93	10.5
789	425	13 000	15 000	W	1.588	13	13.50	13.50	0.20	2.89	3.07
1 630	834	30 000	36 000	J	2.381	12	13.50	13.50	0.30	5.88	6.22
2 460	1 170	28 000	33 000	J	3.175	10	14.00	15.00	0.30	10.9	11.8
797	465	11 000	13 000	W	1.588	14	16.50	16.50	0.20	3.43	3.64
1 760	1 010	26 000	31 000	J	2.381	14	16.50	16.50	0.30	6.86	7.27
1 760	1 010	26 000	31 000	J	2.381	14	16.50	16.50	0.30	9.71	—
3 680	1 800	24 000	29 000	J	3.969	10	17.00	18.50	0.30	16.0	17.1

- (1) Open bearings have shield/seal grooves.
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- (3) Applicable only for open, single Z, ZZ, single RU and 2RU types in inner ring rotating conditions. Limiting speeds for the contact rubber seal(s) types can be lower than the above-mentioned values, so please check the detailed values per item on "products" section of our website.
- (4) Some items are also available with the TW cage. Please contact us for details.

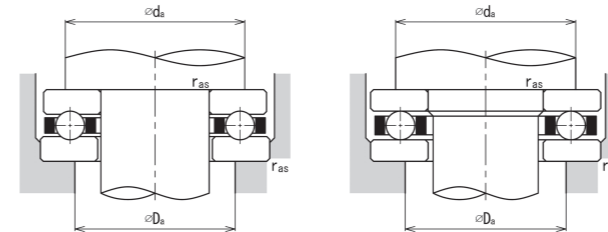
Dimension Flanged extra-thin-section bearings [Stainless-steel]

Thrust bearings



FM (with raceways)

F (without raceways)



Abutment and fillet

FM series (with raceways)

Bore diameter d		Outer diameter D		Outer ring inner diameter d ₁		Inner ring outer diameter D ₁		Chamfer r _s (min)		Height H		Bearing number	Load rating		Limiting speed	Cage type
mm	inch	mm	inch	mm	inch	mm	inch	mm	inch	mm	inch		C _a	C _{0a}	Oil	
													(N)	min ⁻¹		
3	0.1181	8	0.3150	3.2	0.1260	7.8	0.3071	0.15	0.0059	3.5	0.1378	F3-8M	994	932	24 000	TP
4	0.1575	9	0.3543	4.2	0.1654	8.8	0.3465	0.15	0.0059	4.0	0.1575	F4-9M	945	932	22 000	TP
		10	0.3937	4.2	0.1654	9.8	0.3858	0.15	0.0059	4.0	0.1575	F4-10M	925	932	21 000	TP
5	0.1969	12	0.4724	5.2	0.2047	11.8	0.4646	0.20	0.0079	4.0	0.1575	F5-12M	1 060	1 240	19 000	TP
6	0.2362	12	0.4724	6.2	0.2441	11.8	0.4646	0.20	0.0079	4.5	0.1772	F6-12M	1 820	2 220	18 000	TP
		14	0.5512	6.25	0.2461	13.8	0.5433	0.20	0.0079	5.0	0.1969	F6-14M	2 160	2 440	16 000	TP
7	0.2756	13	0.5118	7.2	0.2835	12.8	0.5039	0.20	0.0079	4.5	0.1772	F7-13M	1 770	2 220	18 000	TP
		17	0.6693	7.2	0.2835	16.8	0.6614	0.30	0.0118	6.0	0.2362	F7-17M	3 090	3 800	14 000	TP
8	0.3150	16	0.6299	8.2	0.3228	15.8	0.6220	0.30	0.0118	5.0	0.1969	F8-16M	3 920	4 990	16 000	TP
		19	0.7480	8.2	0.3228	18.8	0.7402	0.30	0.0118	7.0	0.2756	F8-19M	3 940	4 970	12 000	TP
9	0.3543	20	0.7874	9.2	0.3622	19.8	0.7795	0.30	0.0118	7.0	0.2756	F9-20M	3 860	4 970	12 000	TP
10	0.3937	18	0.7087	10.2	0.4016	17.8	0.7008	0.30	0.0118	5.5	0.2165	F10-18M	2 470	3 490	14 000	TP

Ball		Abutment and fillet dimensions			Mass (Ref.)
Size	Qty.	d _a min	D _a max	r _{as} max	
mm	pcs.	mm			g
1.588	6	6.00	5.00	0.15	0.84
1.588	6	7.00	6.00	0.15	1.17
1.588	6	7.60	6.40	0.15	1.49
1.588	8	9.20	7.80	0.20	2.10
2.000	9	9.60	8.40	0.20	2.20
2.381	7	10.80	9.20	0.20	3.54
2.000	9	10.60	9.40	0.20	2.42
2.778	8	13.00	11.00	0.30	6.32
3.000	9	12.80	11.20	0.30	3.94
3.175	8	14.60	12.40	0.30	9.27
3.175	8	15.60	13.40	0.30	9.86
2.381	10	14.80	13.20	0.30	5.34

F series (without raceways)

Bore diameter d		Outer diameter D		Chamfer r _s (min)		Height H		Bearing number	Load rating		Cage type	Ball		Abutment and fillet dimensions		
mm	inch	mm	inch	mm	inch	mm	inch		C _a	C _{0a}		Size	Qty.	d _a min	D _a max	r _{as} max
										(N)		mm	pcs.	mm	mm	mm
2	0.0787	6	0.2362	0.10	0.0039	3.0	0.1181	F2-6	143	83	TD	6	1.000	4.40	3.60	0.10
3	0.1181	8	0.3150	0.10	0.0039	3.5	0.1378	F3-8	212	140	TD	7	1.200	6.00	5.00	0.10
4	0.1575	9	0.3543	0.15	0.0059	4.0	0.1575	F4-9	220	160	TD	8	1.200	7.00	6.00	0.15
		10	0.3937	0.15	0.0059	4.5	0.1772	F4-10	355	245	TD	7	1.588	7.60	6.40	0.15
5	0.1969	11	0.4331	0.15	0.0059	4.5	0.1772	F5-11	341	245	TD	7	1.588	8.60	7.40	0.15
6	0.2362	12	0.4724	0.15	0.0059	4.5	0.1772	F6-12	389	314	TD	9	1.588	9.60	8.40	0.15
7	0.2756	15	0.5906	0.20	0.0079	5.0	0.1969	F7-15	793	628	TD	8	2.381	11.80	10.20	0.20
8	0.3150	16	0.6299	0.20	0.0079	5.0	0.1969	F8-16	537	443	TD	8	2.000	12.70	11.10	0.20
9	0.3543	17	0.6693	0.20	0.0079	5.0	0.1969	F9-17	567	499	TD	9	2.000	13.70	12.10	0.20
10	0.3937	18	0.7087	0.20	0.0079	5.5	0.2165	F10-18	800	707	TD	9	2.381	14.70	13.10	0.20

Mass (Ref.)
g
0.50
1.03
1.39
1.94
2.22
2.49
4.24
4.88
5.25
6.11

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: ISO 14001 : JQA-EM0554

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